



Mitigation of the ZDR Bias Temperature Dependence

Frank Gekat, Markus Hille, Markus Krings

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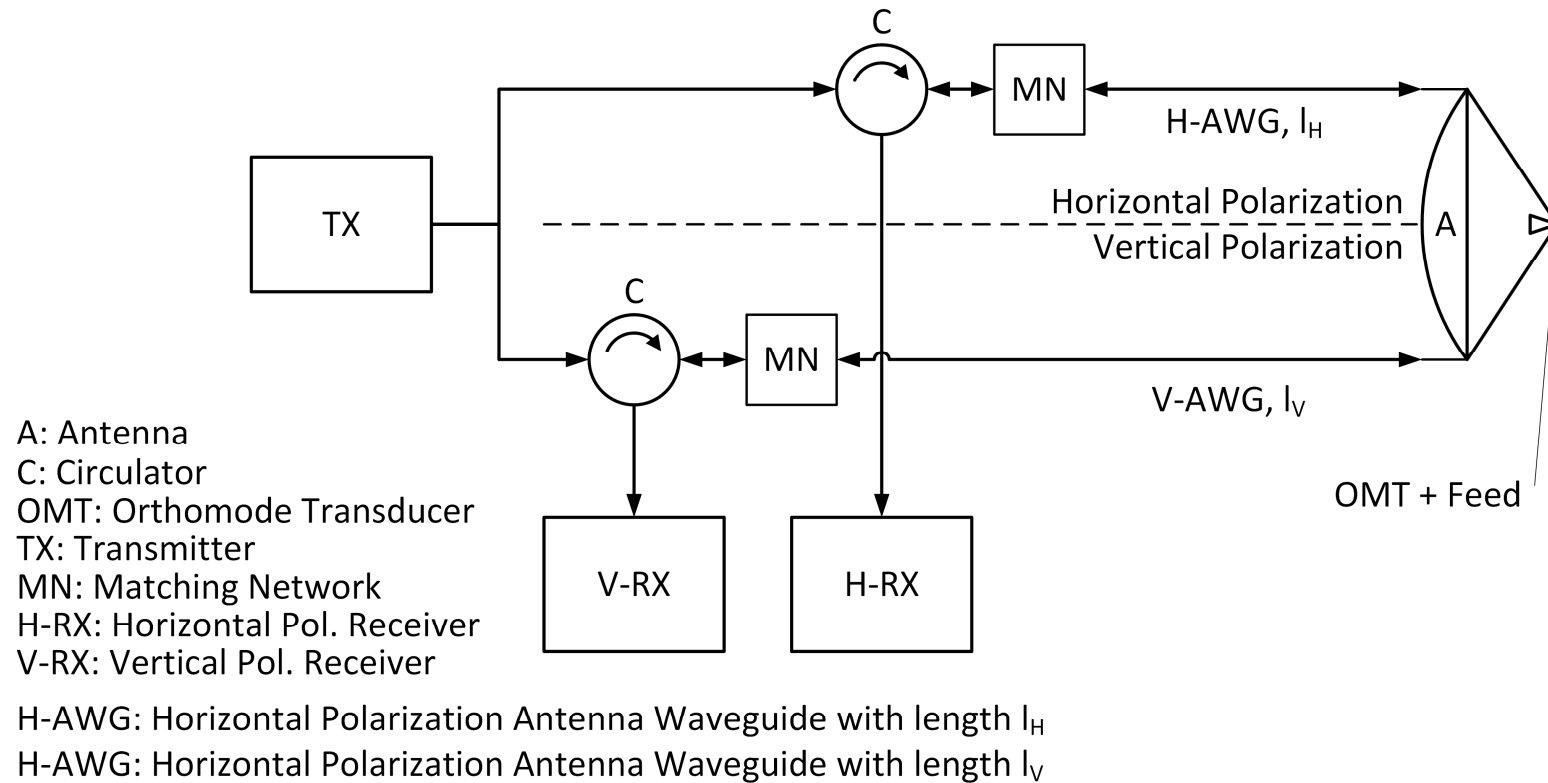


INTRODUCTION

- It is well known that the ZDR Bias of a polarimetric weather radar shows a dependence on the outdoor temperature see e.g. (1) and (2) (0.2 dB over 12 °C temperature change (1))
- The root cause(s) of this temperature-dependent variance is yet unknown. In most publications it is speculated that it could be the antenna
- In this talk we will show that one possible reason could be the difference in the thermal variations of the horizontal and vertical polarization waveguide circuits between the radar and the antenna
- We will also propose a simple approach to mitigate the effects of these variations
- Furthermore we will indicate some other radar parameters which might have a similar effect



SIMPLIFIED BLOCK DIAGRAM OF A POLARIMETRIC WEATHER RADAR





ANTENNA WAVEGUIDE AS A RESONATOR

Resonance frequencies of a TE_{10n} cavity (3)

$$f_r = \frac{c}{2\pi} \sqrt{\left(\frac{\pi}{a(T)}\right)^2 + \left(\frac{n\pi}{l(T)}\right)^2}$$

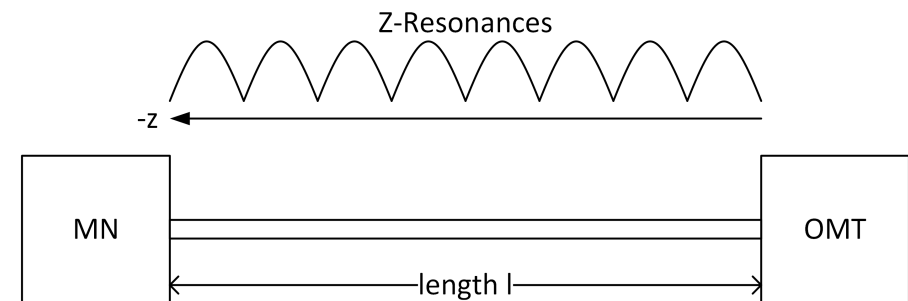
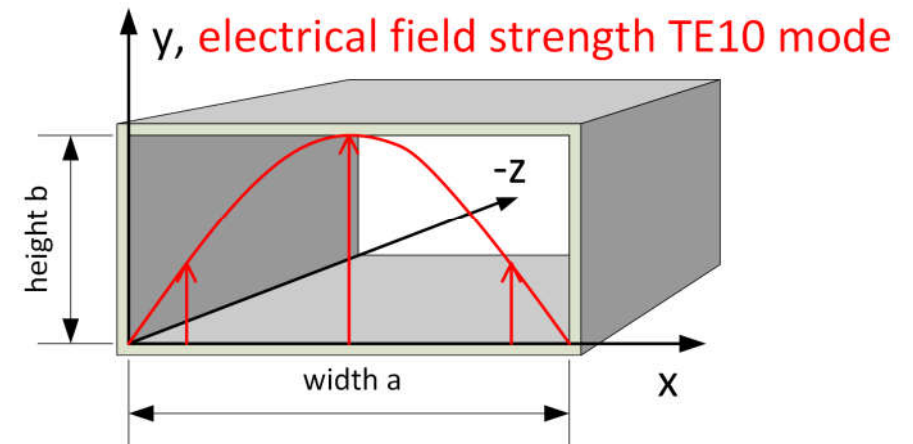
c: speed of light, n: integer, T: temperature

Thermal variations

$$a(T) = a_0(1 + \alpha\Delta T)$$

$$l(T) = l_0(1 + \alpha\Delta T)$$

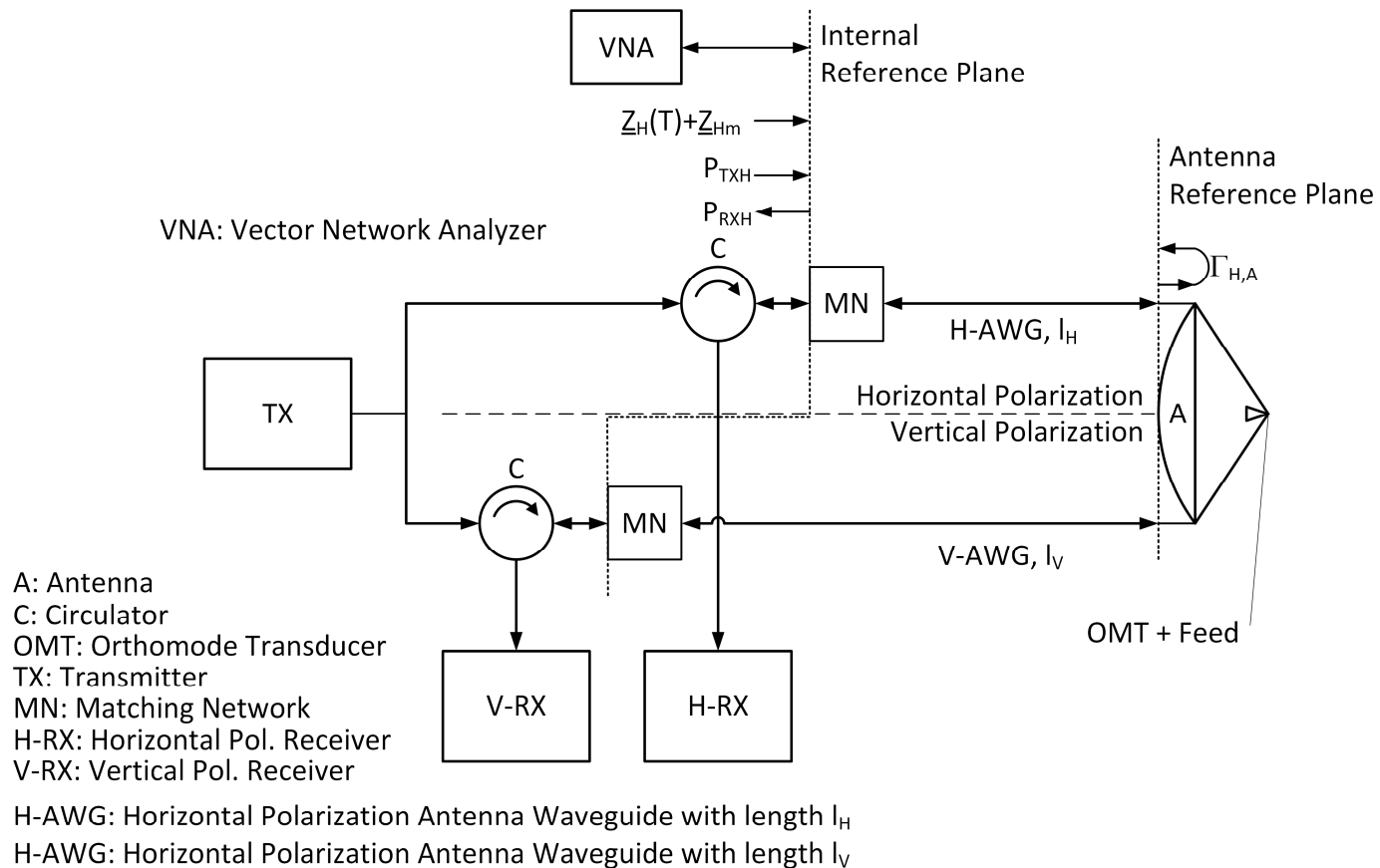
Thermal expansion coefficient of Aluminum: $\alpha_{Al} = 23.1 \cdot 10^{-6} \text{ K}^{-1}$



Wave-guide	Frequency	Width a	Thermal Coefficient	
			Length l, 25 m	Length l, 5 m
WR284	2800 MHz	72.14 mm	-64.71 kHz/K	-64.43 kHz/K
WR187	5640 MHz	47.55 mm	-130.23 kHz/K	-129.77 kHz/K



RETURN LOSS AT THE INPUT OF THE MATCHING NETWORK





CALCULATION OF THE RETURN LOSS AT THE INPUT OF THE MATCHING NETWORK

Waveguide wavelength

$$\lambda_g(T) = \lambda / \sqrt{1 - (\lambda / 2a(T))^2}$$

Waveguide phase constant

$$\beta(T) = 2\pi / \lambda_g(T)$$

OMT impedance

$$\underline{Z}_A = (1 + \underline{\Gamma}_A) / (1 - \underline{\Gamma}_A)$$

$\underline{\Gamma}_A$: complex OMT reflection coefficient

All equations from Ref. (4)

Transformed OMT impedance

$$\underline{Z}(T) = Z_0 \frac{\underline{Z}_A + jZ_0 \tan(\beta(T)l(T))}{Z_0 + j\underline{Z}_A \tan(\beta(T)l(T))}$$

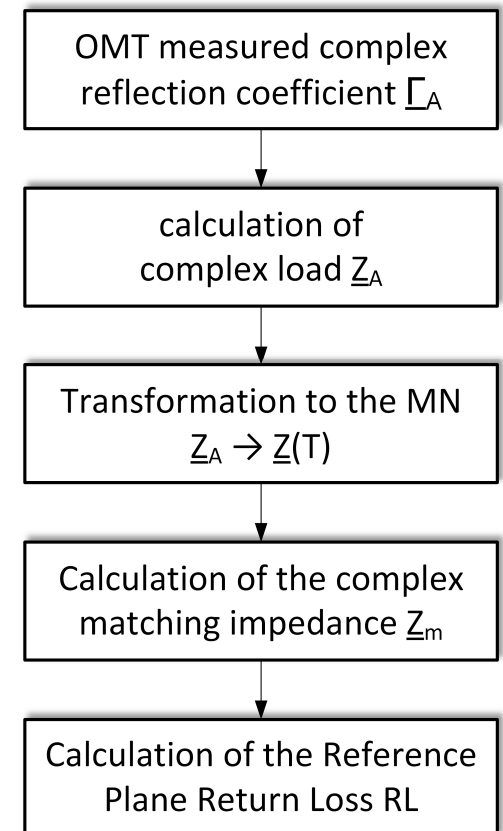
Complex matching impedance

$$\underline{Z}_m = 1 - Re(Z(T_0)) + j(-Im(Z(T_0)))$$

T_0 : outdoor temperature during tuning of MN

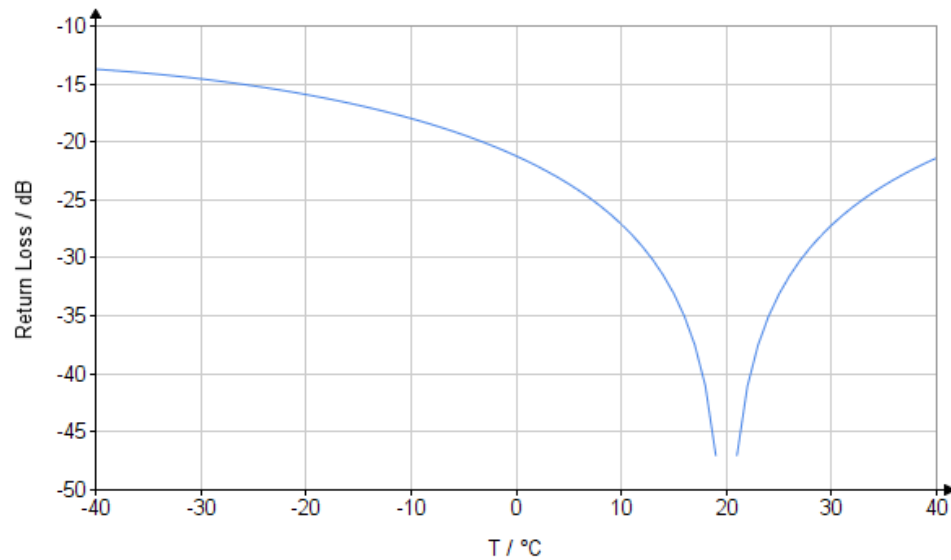
Return Loss in the reference plane

$$RL = \left| \frac{\underline{Z}(T) + \underline{Z}_m - 1}{\underline{Z}(T) + \underline{Z}_m + 1} \right|^2$$

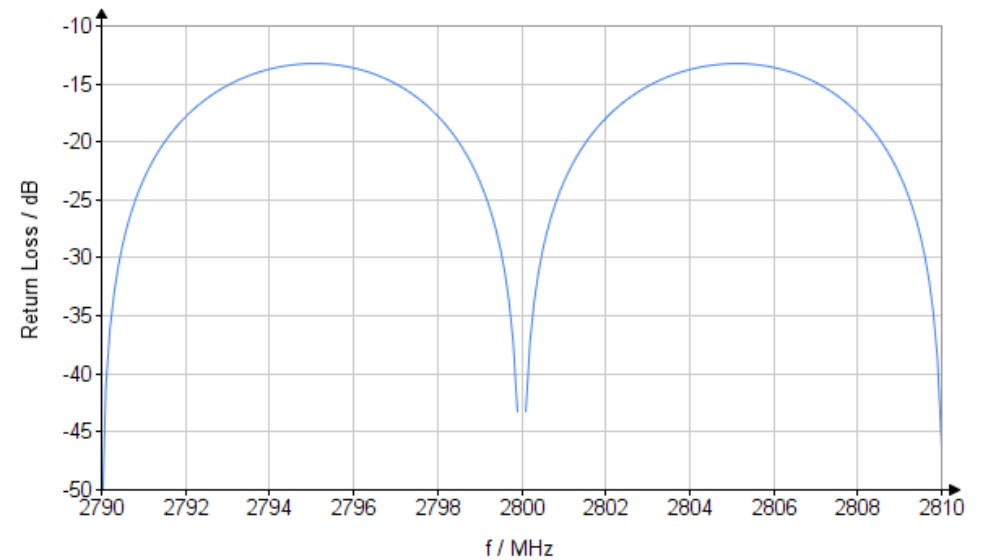




CALCULATION RESULT



Matching Frequency: 2800 MHz
Matching Temperature: 20 °C
Waveguide Length: 10 m



OMT Return Loss: -18 dB
OMT Mismatch Phase: $3\pi/2$

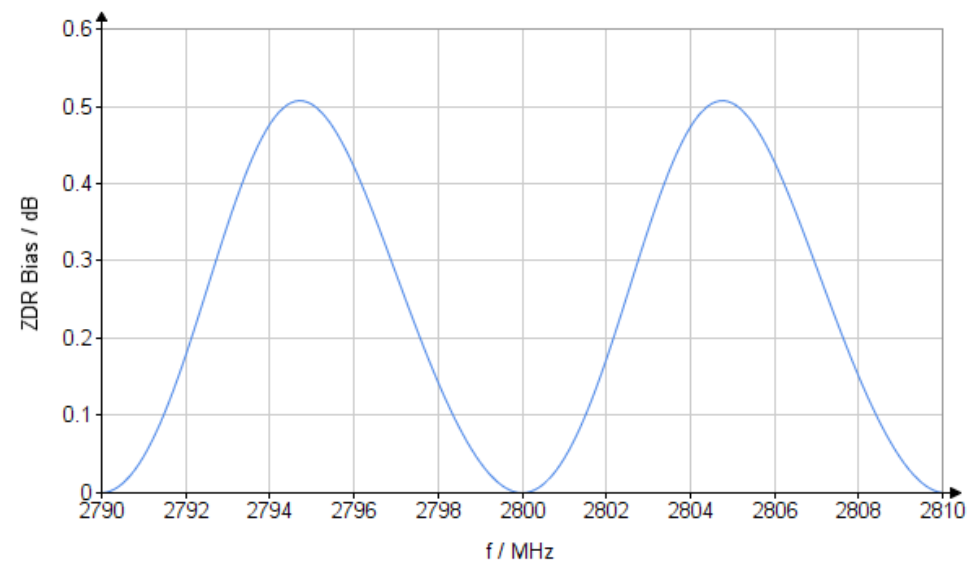
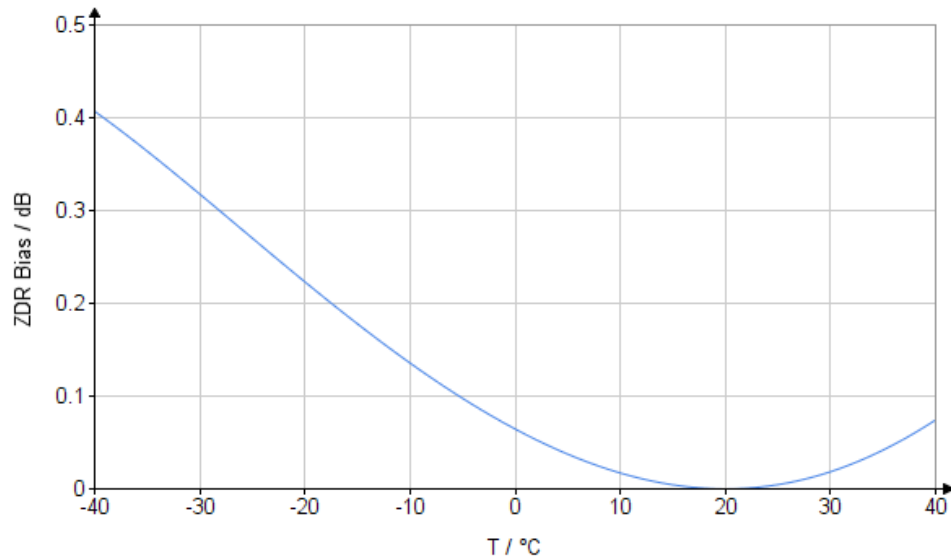


CALCULATION OF THE ZDR BIAS CAUSED BY DIFFERENT RETURN LOSSES

ZDR Bias caused by different return losses of the horizontal and vertical polarization waveguide

$$ZDR_{Bias}(T) = \frac{(1 - RL_H(T))^2}{(1 - RL_V(T))^2}$$

RLmax ≤ -20dB
⇒ max. ZDR Bias ±0.087 dB



Matching Frequency: 2800 MHz
Matching Temperature: 20 °C
Waveguide Length: 10 m

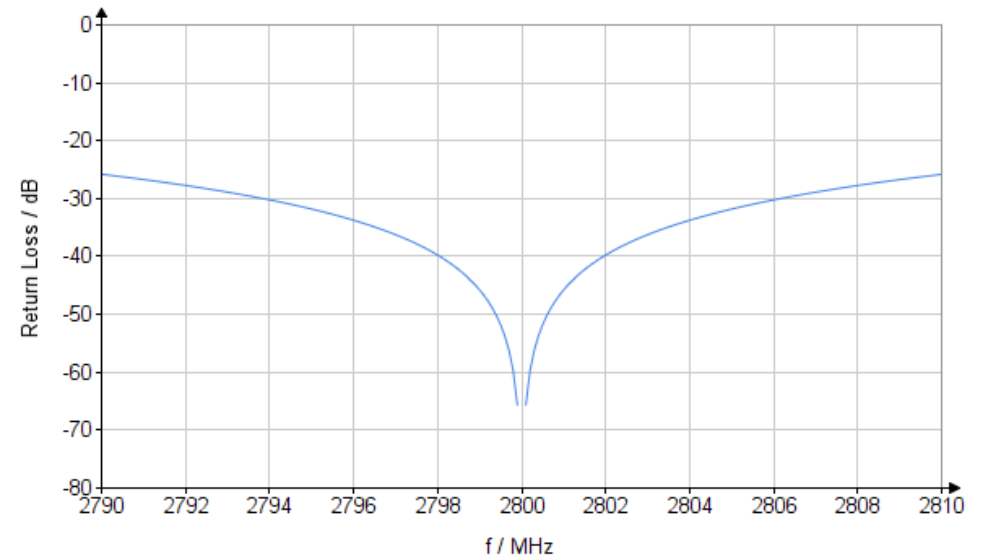
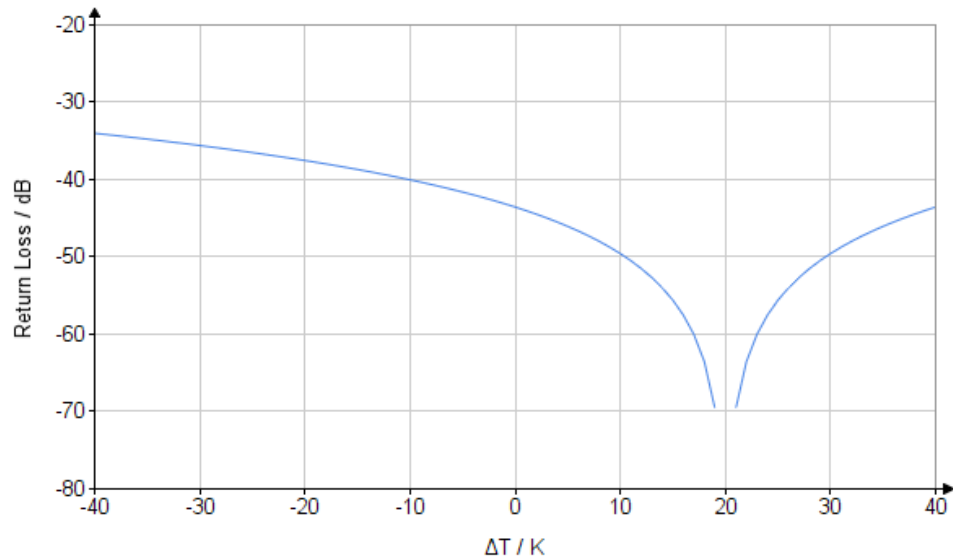
Horizontal Port
Vertical Port

OMT Return Loss: -18 dB OMT Mismatch Phase: 0
OMT Return Loss: -18 dB OMT Mismatch Phase: 3π/2



CALCULATION OF THE ZDR BIAS CAUSED BY DIFFERENT RETURN LOSSES

Short Distance between mismatched load and tuner



Matching Frequency: 2800 MHz

Matching Temperature: 20 °C

Waveguide Length: 0.5 m

Horizontal Port

Vertical Port

OMT Return Loss: -18 dB OMT Mismatch Phase: 0

OMT Return Loss: -18 dB OMT Mismatch Phase: $3\pi/2$



TUNING OF THE ANTENNA WAVEGUIDE / OMT

Design the system in a way that a tuner can be placed as close to the OMT as possible

Measure the temperature coefficient of both (horizontal and vertical polarization) antenna waveguides

- Connect the VNA to the reference plane input port of the respective antenna waveguide
- Measure the reflection coefficient S_{11}
- Set the markers to one or two distinct notches and measure the frequency of the notches
- Wait until the outdoor temperature has changed by at least 10°C
- Repeat the measurement of the frequencies of the notches
- Calculate the temperature coefficient $\frac{\Delta f}{\Delta T} = \frac{f_{notch}(T_{hot}) - f_{notch}(T_{cold})}{T_{hot} - T_{cold}}$ Note that the coefficient is always negative!

Calculate the high frequency limit of the tuning interval $f_{high} = f + \frac{\Delta f}{\Delta T} (T - T_{high})$ T: Temperature during tuning, T_{high} : Max. operating outdoor temperature

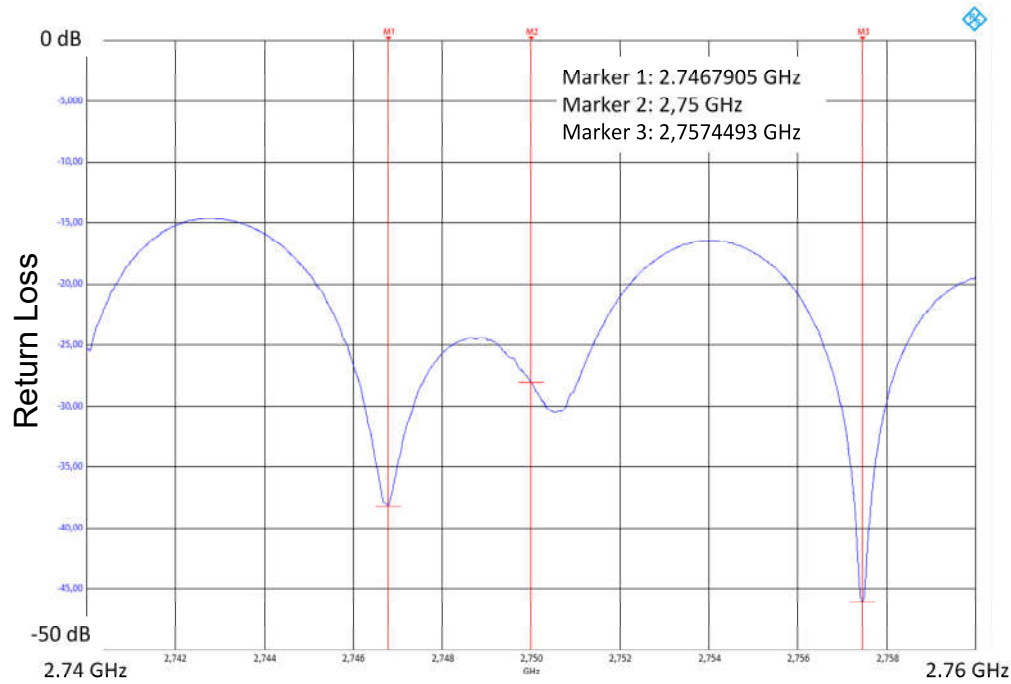
Calculate the low frequency limit of the tuning interval $f_{low} = f + \frac{\Delta f}{\Delta T} (T - T_{low})$ T_{low} : Min. operating outdoor temperature

Tune the waveguide using the VNA display as reference (Set the markers of the VNA to the frequency limits)

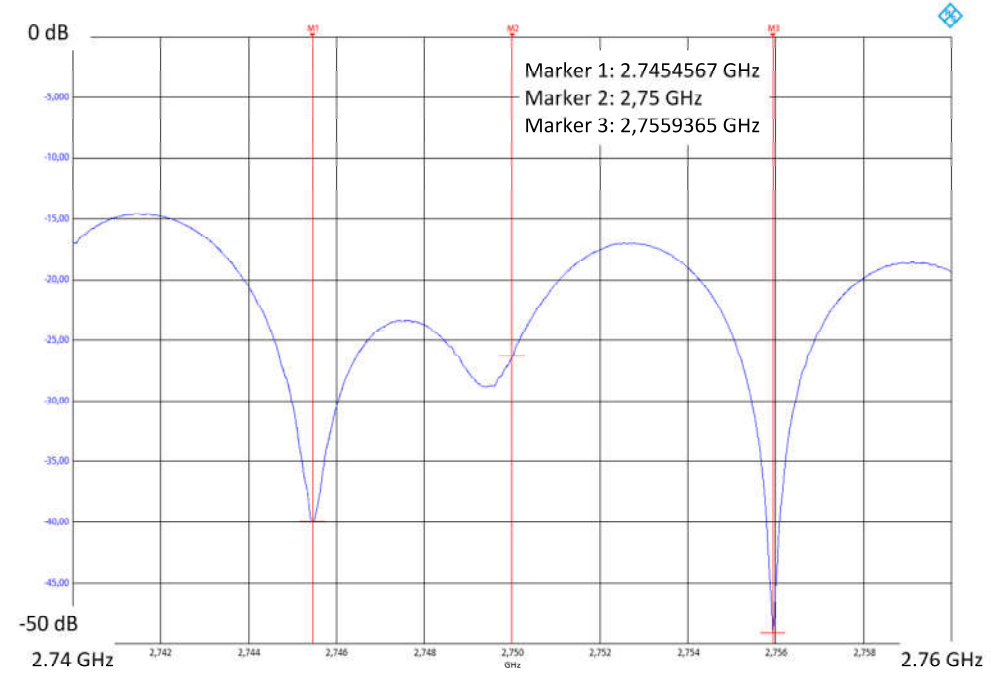


MEASUREMENT OF THE TEMPERATURE COEFFICIENT

$T_{\text{cold}} = 24.8 \text{ }^\circ\text{C}$
 $F_{\text{notch}} = 2.7574493 \text{ GHz}$



$T_{\text{hot}} = 34.8 \text{ }^\circ\text{C}$
 $F_{\text{notch}} = 2.7559365 \text{ GHz}$



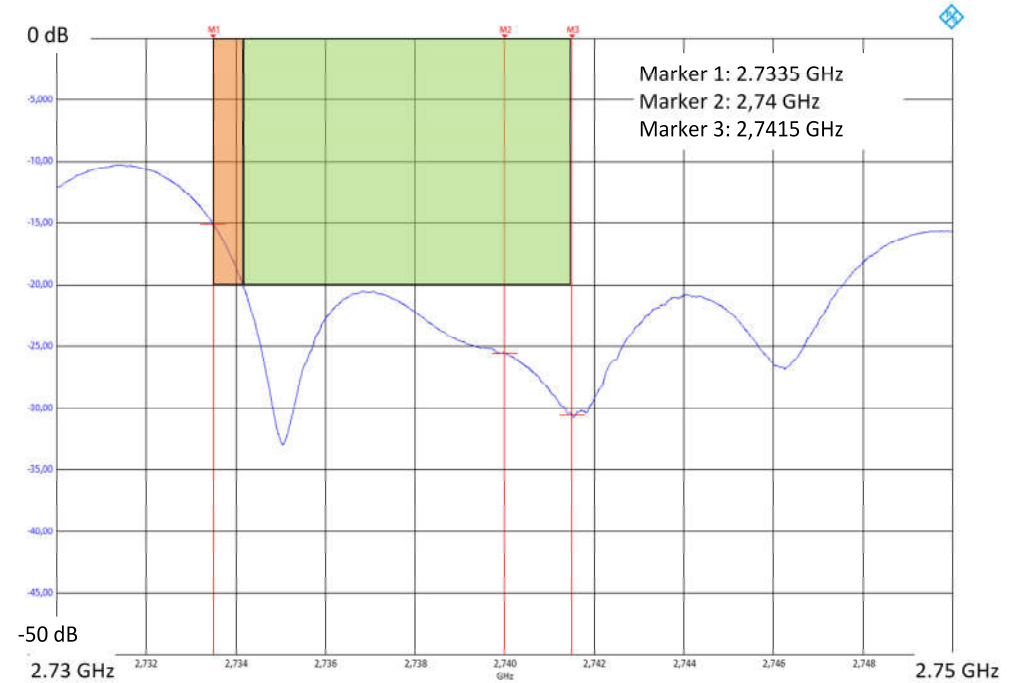
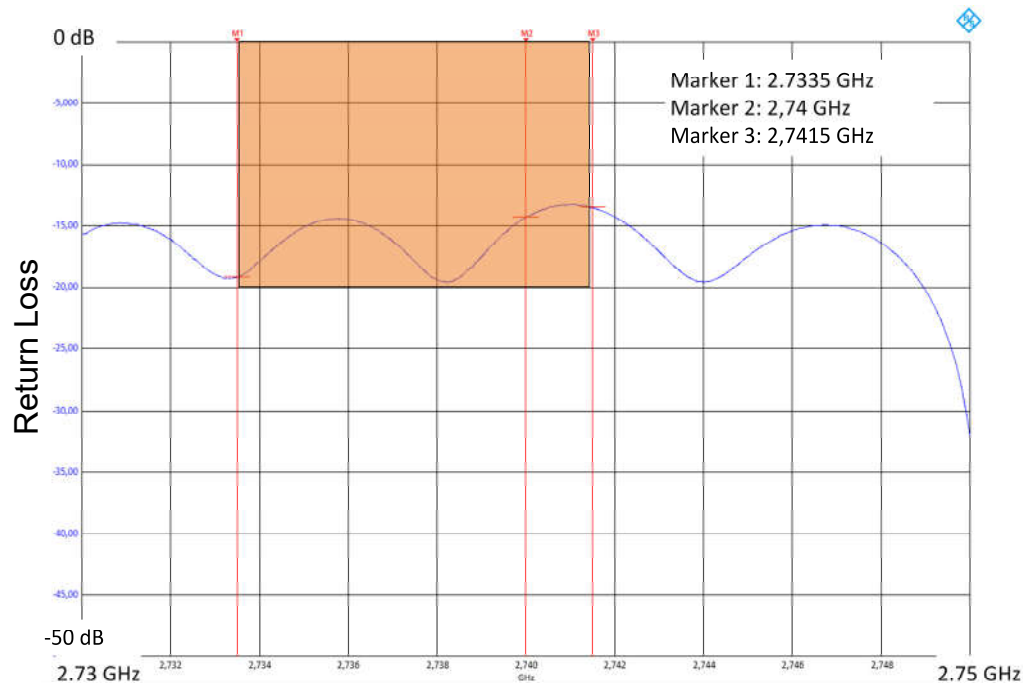
Temperature coefficient $\Delta F/\Delta T = -151 \text{ kHz}/^\circ\text{C}$



TUNING OF HORIZONTAL POLARIZATION ANTENNA WAVEGUIDE

Tuning temperature: 25 °C
Temperature coefficient: 100 kHz/°C
Radar frequency: 2.74 GHz

Outdoor operating temperature: -40 °C - +40 °C
Tuning frequency interval 2.7335 GHz – 2,7415 GHz

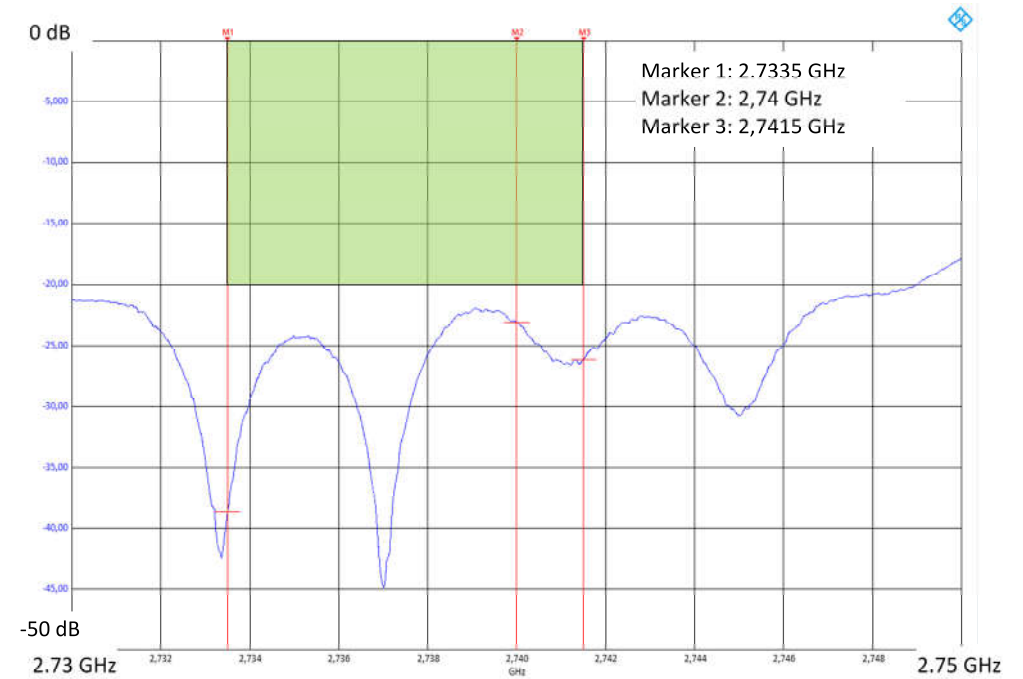
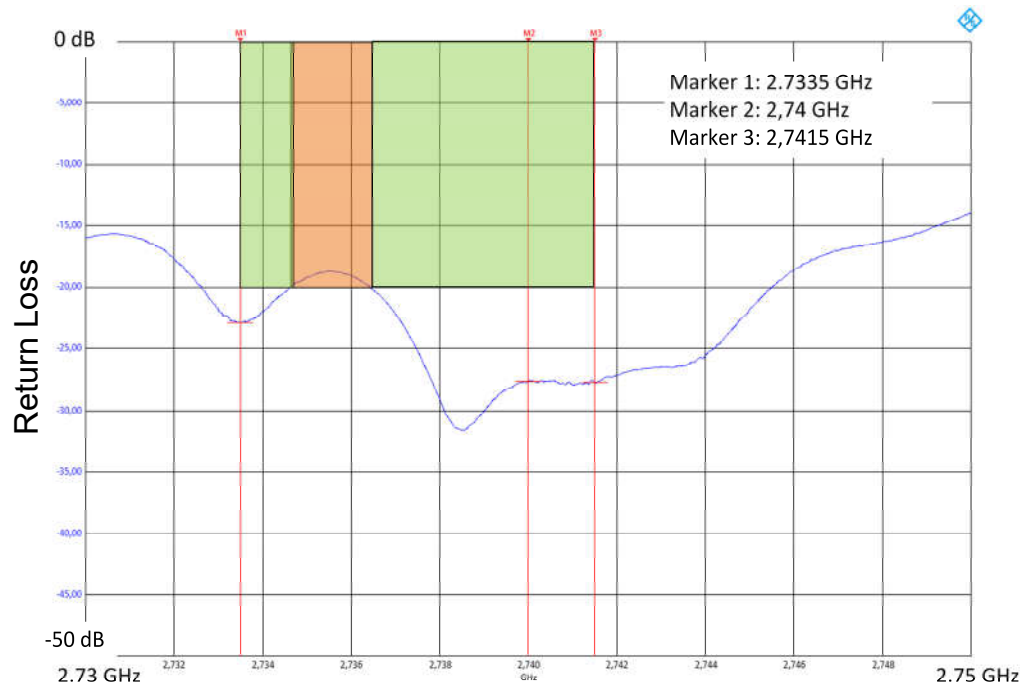




TUNING OF VERTICAL POLARIZATION ANTENNA WAVEGUIDE

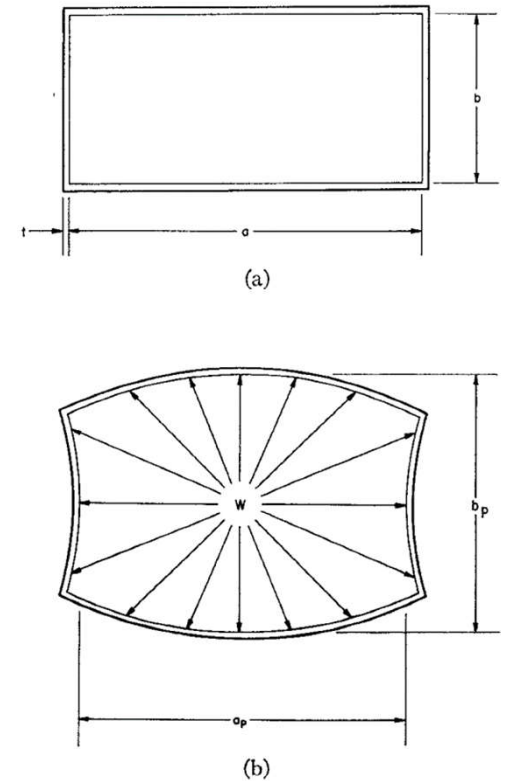
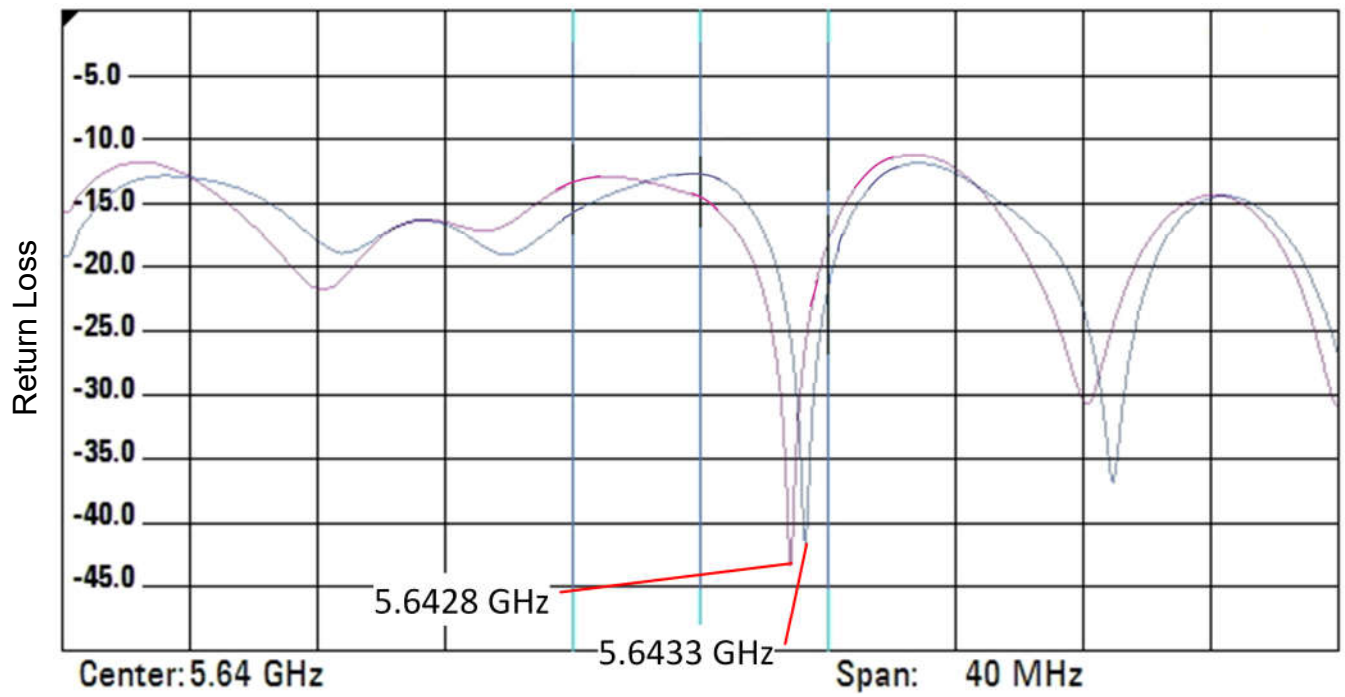
Tuning temperature: 25 °C
Temperature coefficient: 100 kHz/°C
Radar frequency: 2.74 GHz

Outdoor operating temperature: -40 °C - +40 °C
Tuning frequency interval 2.7335 GHz – 2,7415 GHz





PRESSURE DEPENDENCE WAVEGUIDE MATCHING



From Virgile: Deflection of Waveguide Subjected to Internal Pressure (5)

Fig. 1—(a) Unpressurized waveguide; (b) waveguide under pressure.



PRESSURE DEPENDENCE WAVEGUIDE MATCHING

Parameters

$f(0 \text{ mbar}) = 5.6428 \text{ GHz}$

$f(30 \text{ kPa}) = 5.6433 \text{ GHz}$

$a(0 \text{ mbar}) = 47.55 \text{ mm (WR187)}$

$b = 22.15 \text{ mm (WR187)}$

$t = 1.626 \text{ mm (WR187)}$

$E = 69 \text{ GPa}$ Young's Modulus for Al

$w = 30 \text{ kPa}$ waveguide pressure

Calculation based on resonance frequency

Resonance frequencies of a TE_{10n} cavity:

$$f_r = \frac{c}{2\pi} \sqrt{\left(\frac{\pi}{a(p)}\right)^2 + L^2}$$

Calculate L^2 using $f(0 \text{ mbar})$ and $a(0 \text{ mbar})$

Calculate $a(430 \text{ mbar})$ using $f(430 \text{ mbar})$ and L^2

$$\Delta a = a(30\text{kPa}) - a = -13.5 \mu\text{m}$$

Calculation based on deflection theory

From Virgile: Deflection of Waveguide Subjected to Internal Pressure (5):

$$y_b = \frac{w}{E} \left(\frac{5}{32} \frac{b^4}{t^3} - \frac{b^2(a^3+b^3)}{8(a+b)t^3} \right)$$

$$a_p = a + 2y_b, \quad \Delta a = a_p - a$$

$$\Delta a = 13.46 \mu\text{m}$$



SUMMARY

ZDR bias variations can be caused by:

- Temperature variations of the antenna waveguide circuit
- Transmitter frequency drift or modulation
- Variation of the waveguide pressure
- All parameters mentioned above affect the horizontal and vertical polarization antenna waveguide in the same manner. However due to slight differences in the length and residual mismatches of both waveguides the ZDR bias varies due to the variation of the transformation of these mismatches.



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Thank you for your attention!

Frank Gekat

f.gekat@leonardogermany.com

LEONARDO Germany GmbH
Raiffeisenstrasse 10
41470 Neuss, Germany
Tel: +49 (0) 2137 782-0
info@leonardogermany.com
www.leonardogermany.com