

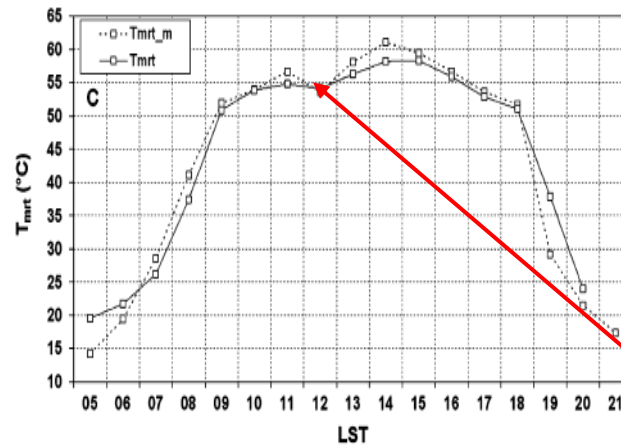
# Mean radiant temperature

$$T_{mrt}$$

Temperature of a standing man in  
radiative balance (short- and longwave)  
with his surrounding

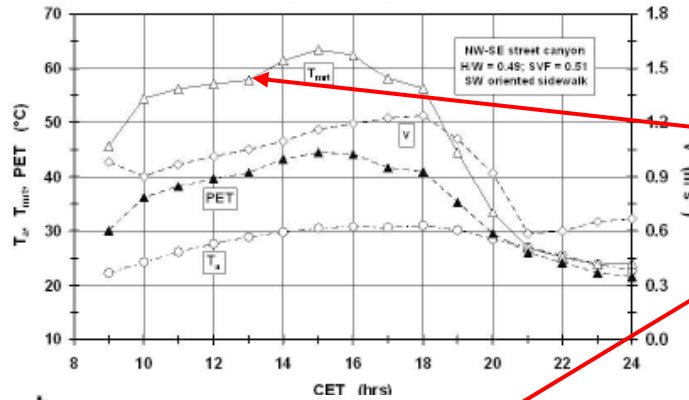


Lindberg et al. 2008  
(model and obs)



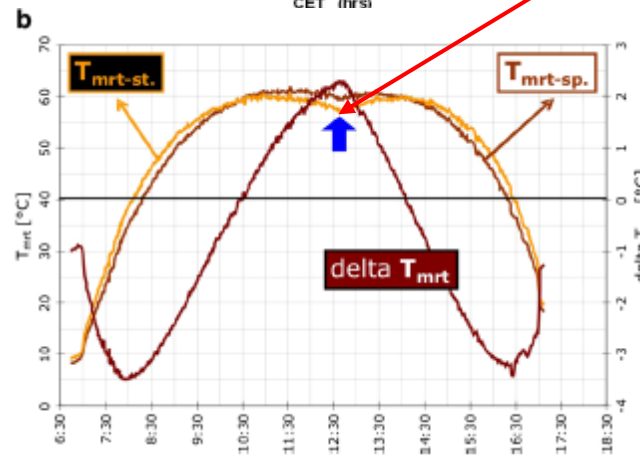
# The problem

Mayer et al. 2008  
(obs)

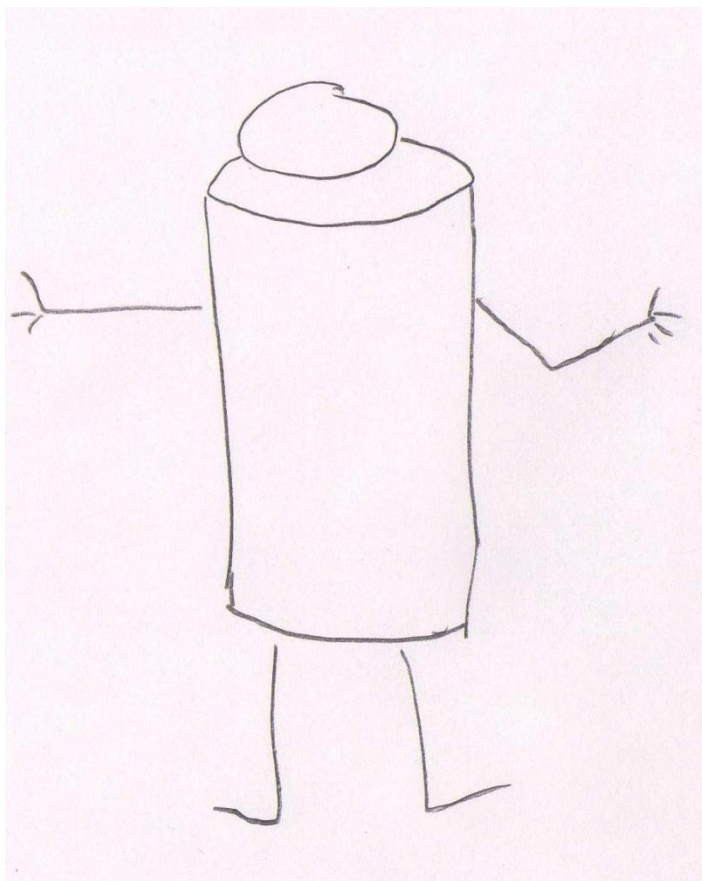


A local minimum  
around noon

Kantor et al. 2014  
(obs)

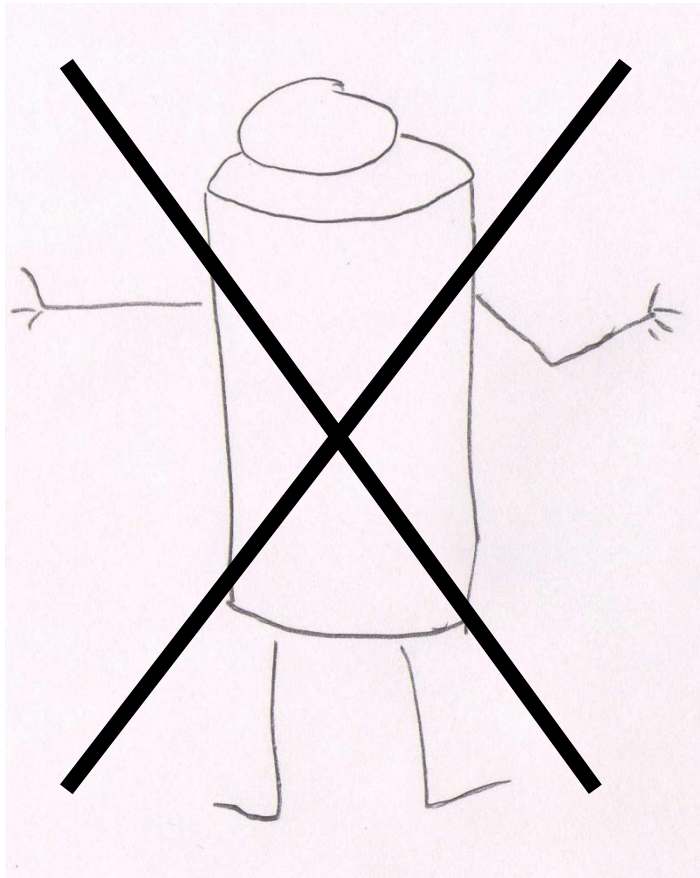


# Mr. Cylinder

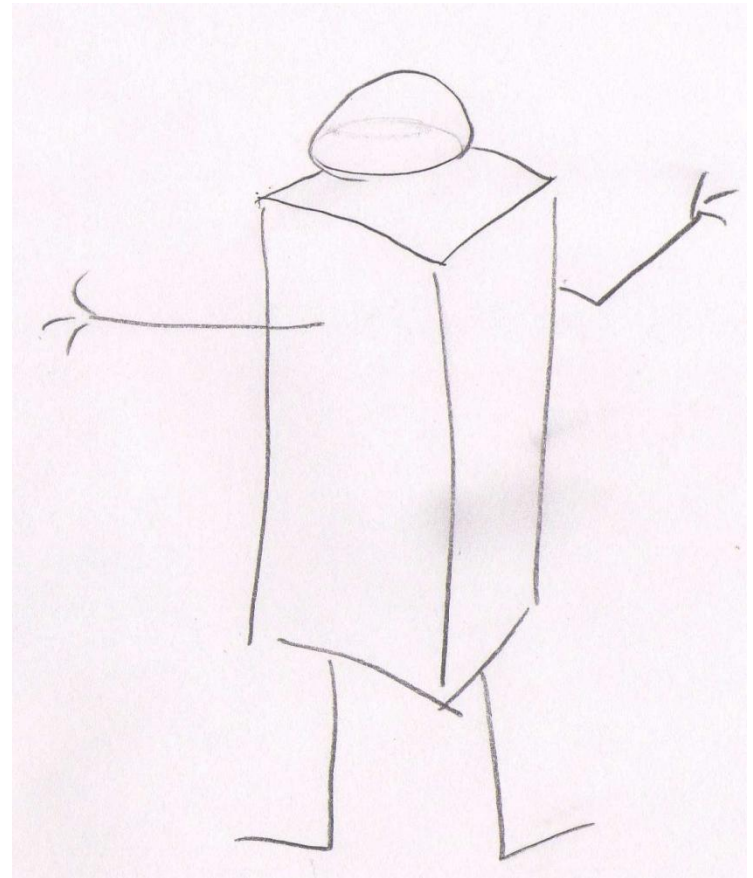


**But!!** - "... the “standing man” reference shape is in fact a rectangular column and not a rotationally symmetric cylinder.”  
(Kantor et al. 2014)

Mr. Cylinder



Mr. Box



**How to transform the standing man from a box to a cylinder  
– a modified methodology to calculate mean radiant  
temperature in field studies and models**

Björn Holmer, Fredrik Lindberg, David Rayner, Sofia Thorsson

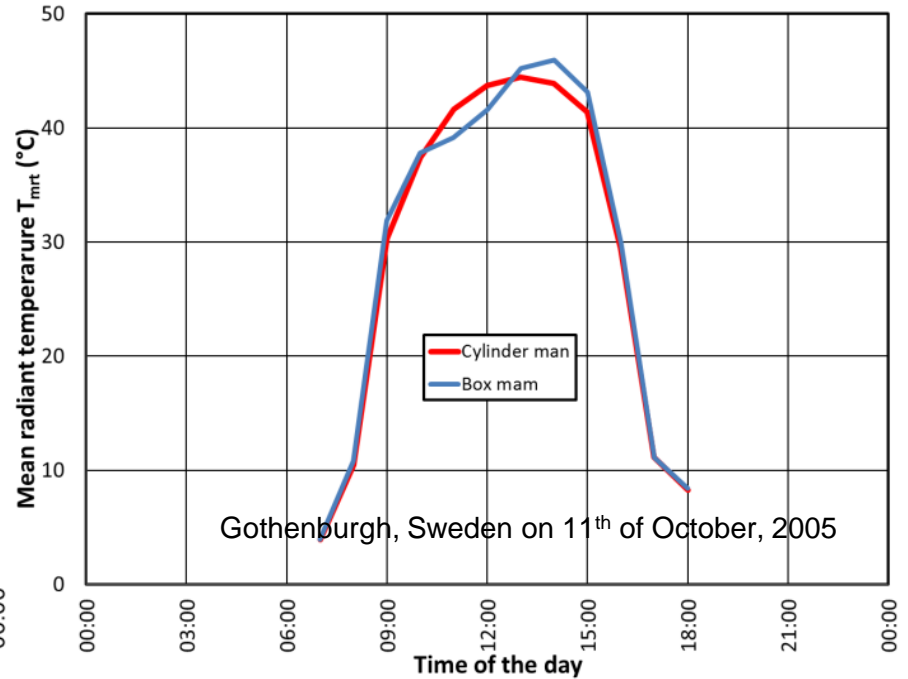
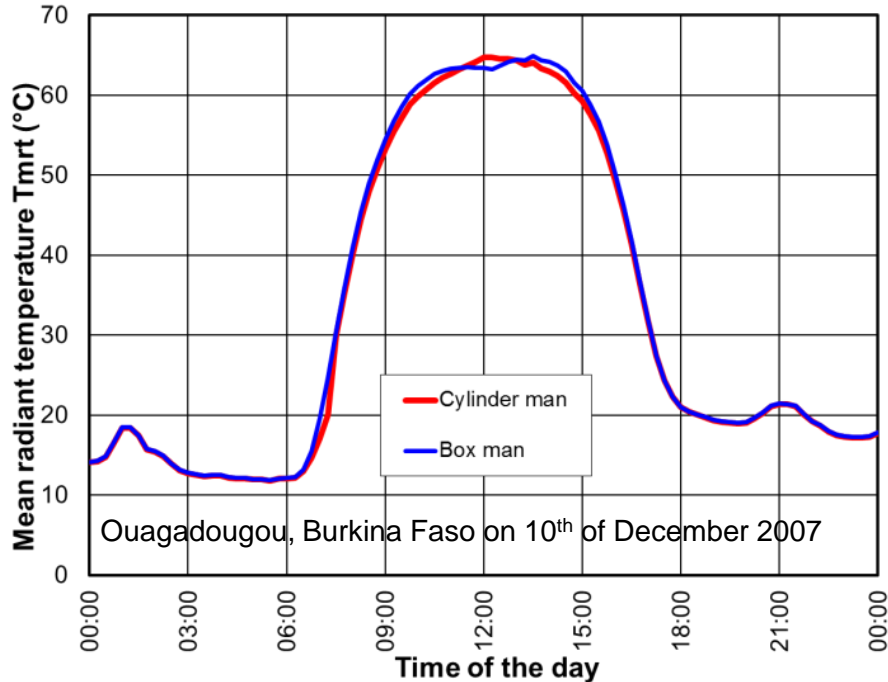
*Urban Climate Group, Dept of Earth Sciences  
University of Gothenburg, Sweden*

- The solution is connected to the area that is exposed to the direct short-wave radiation

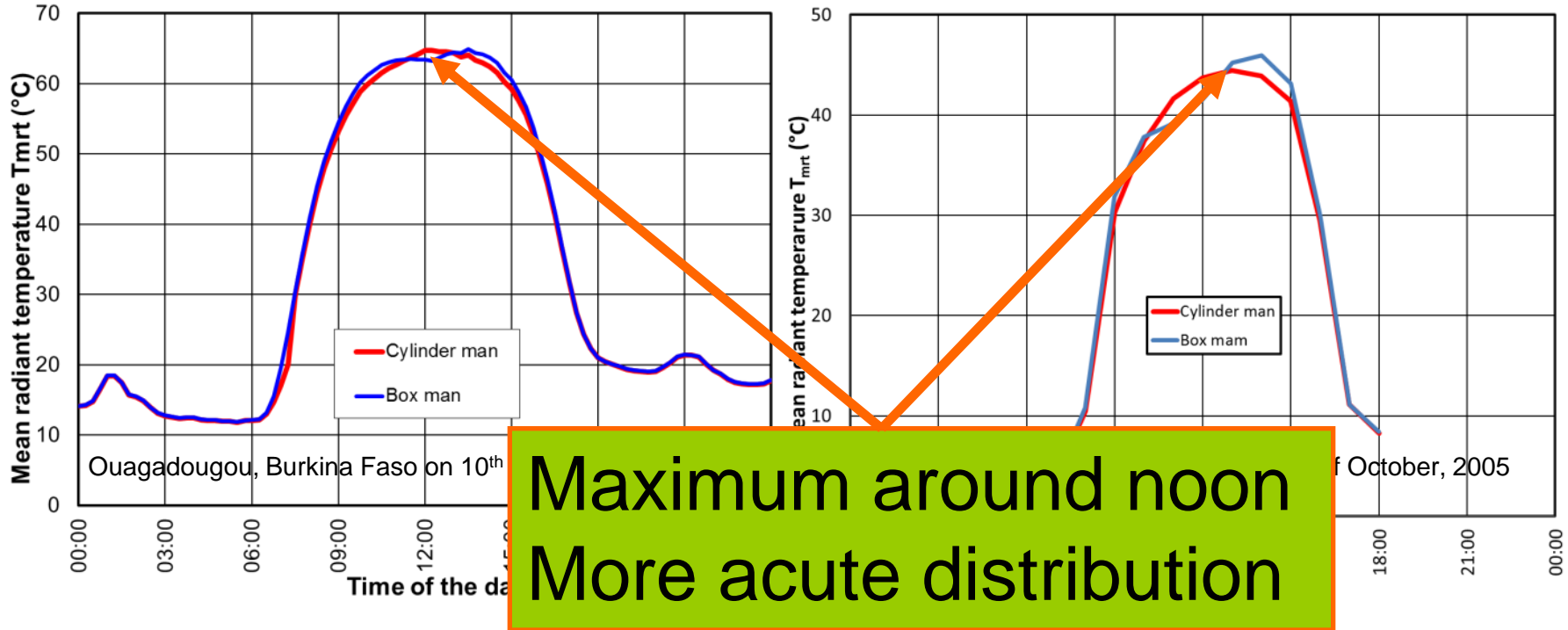
# Comparison of old and new calculation

*Box man - the original formula by Höppe*

*Cylinder man - the new methodology*



# Comparison of old and new calculation



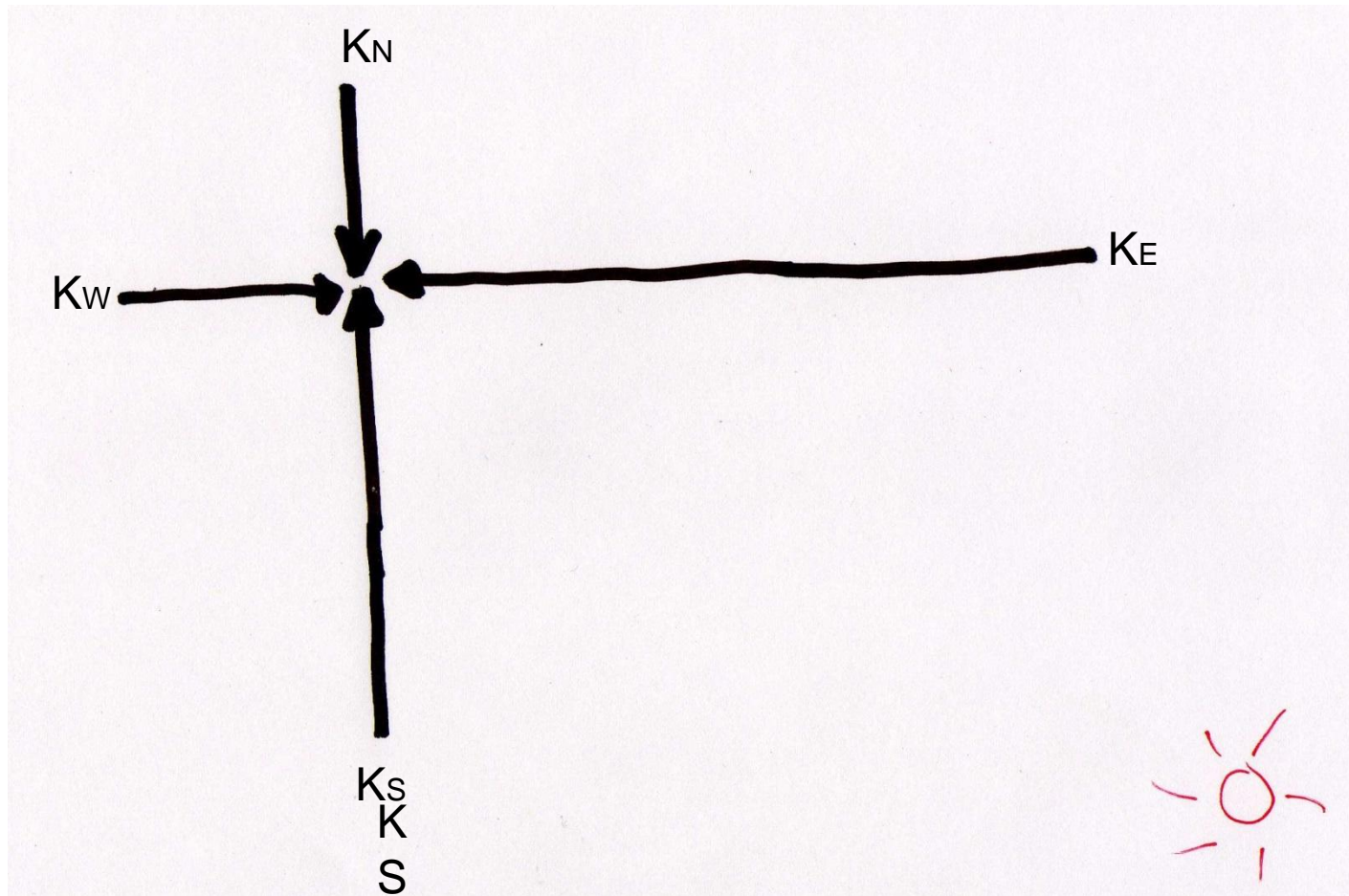
*Box man - the original formula by Höppe*

*Cylinder man - the new methodology*

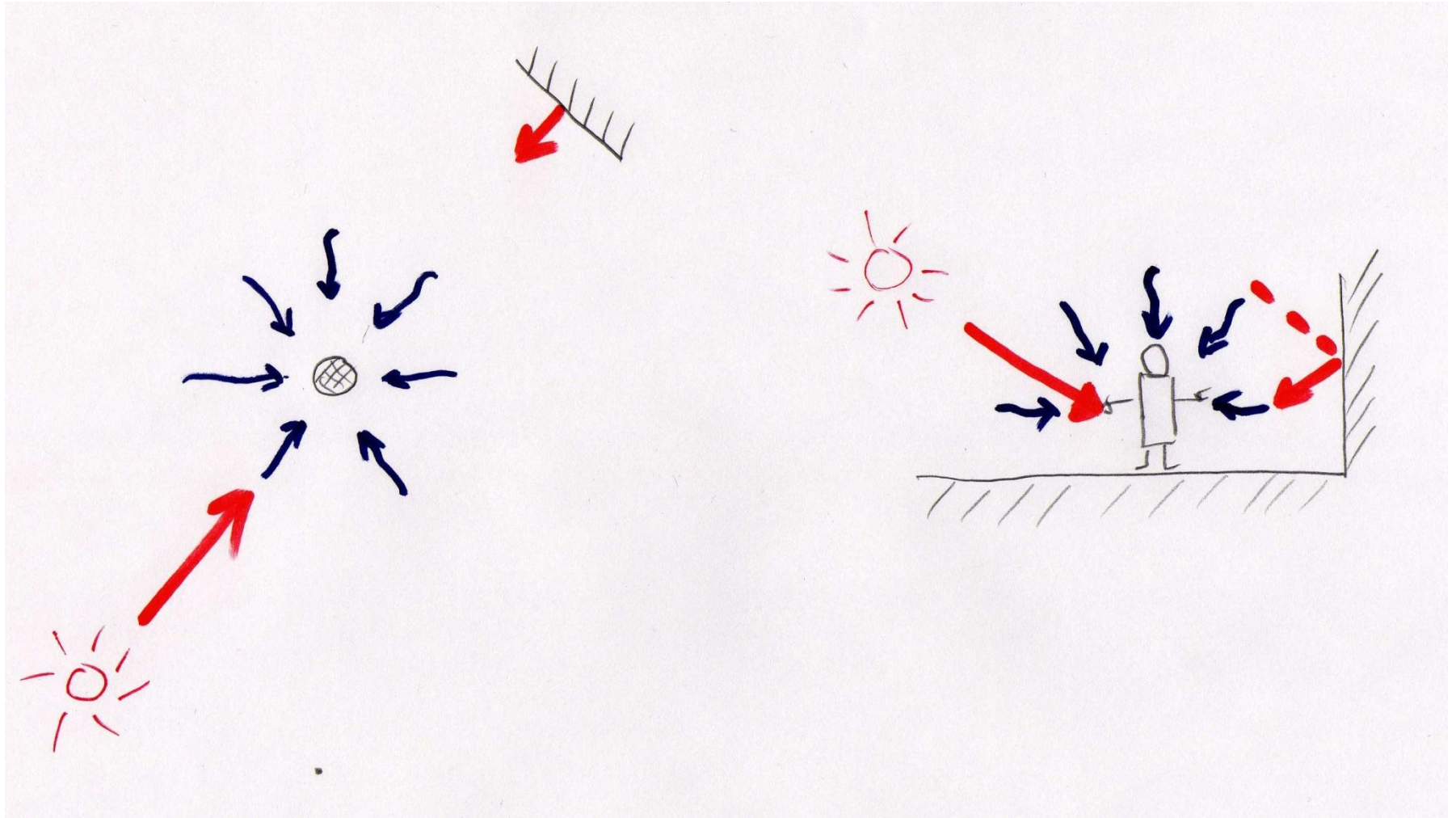
# Six directional measurements



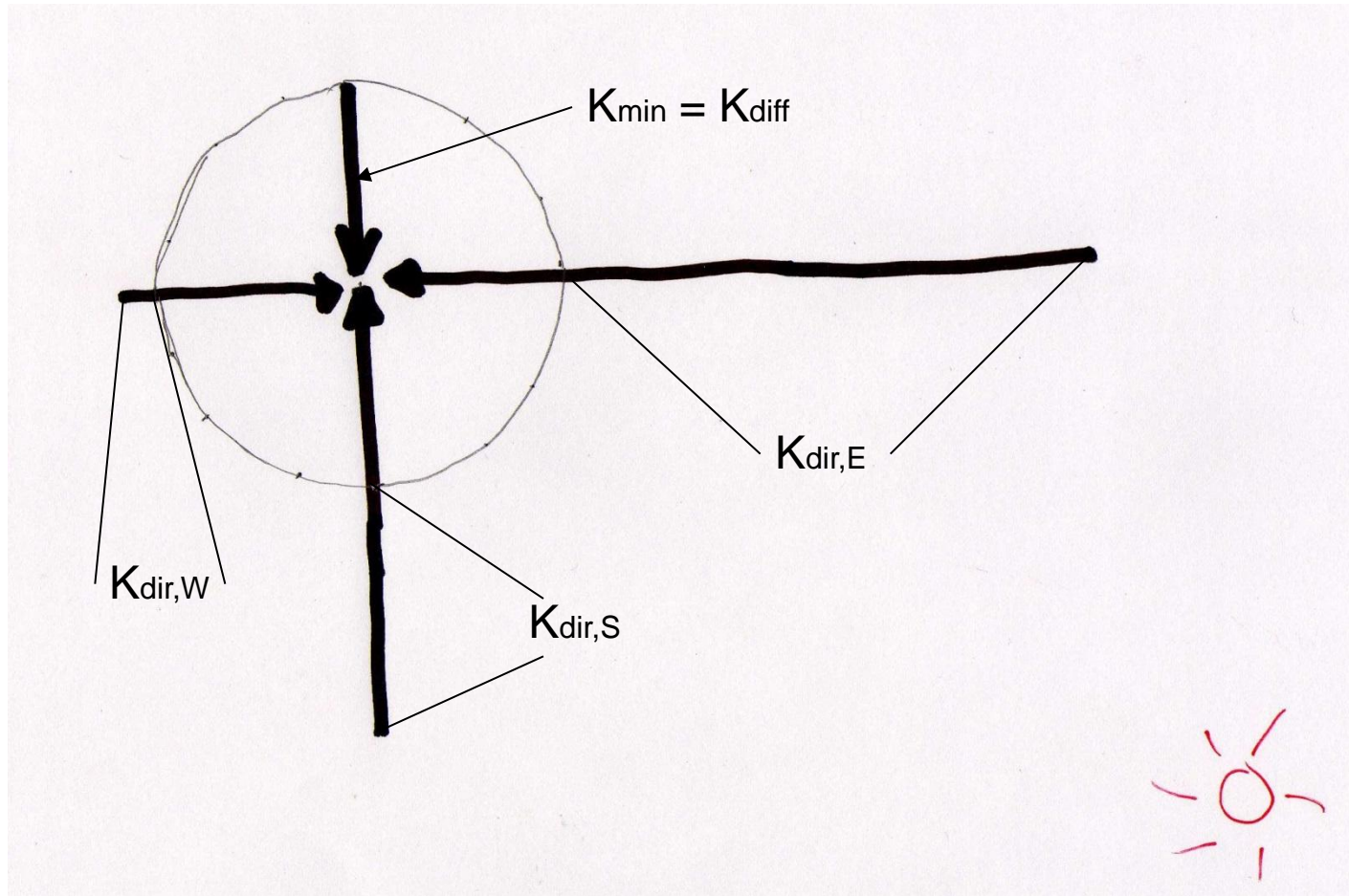
# Recorded horizontal short-wave radiation



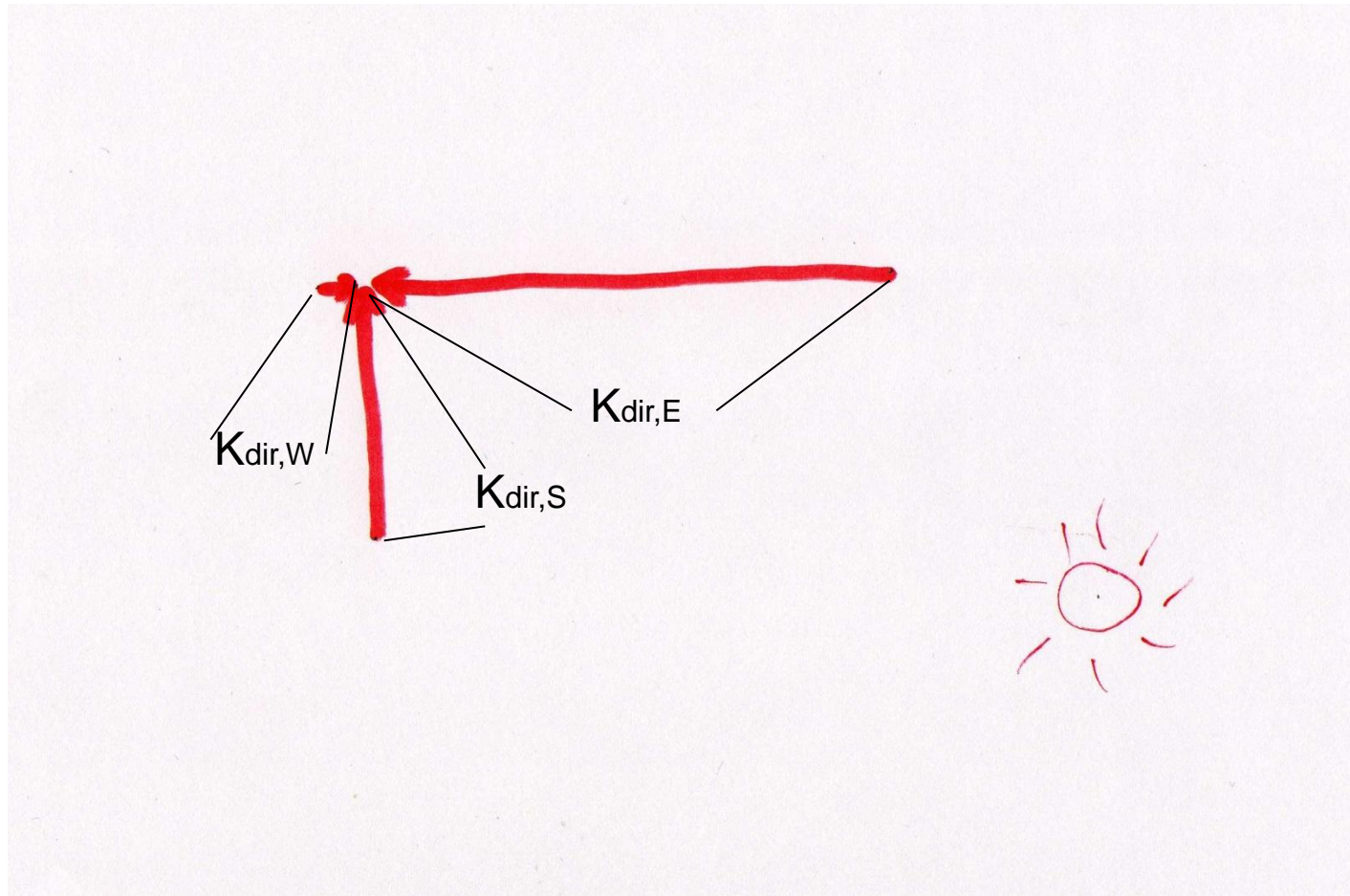
# Direct and diffuse short-wave radiation



# Horizontal diffuse and direct radiation

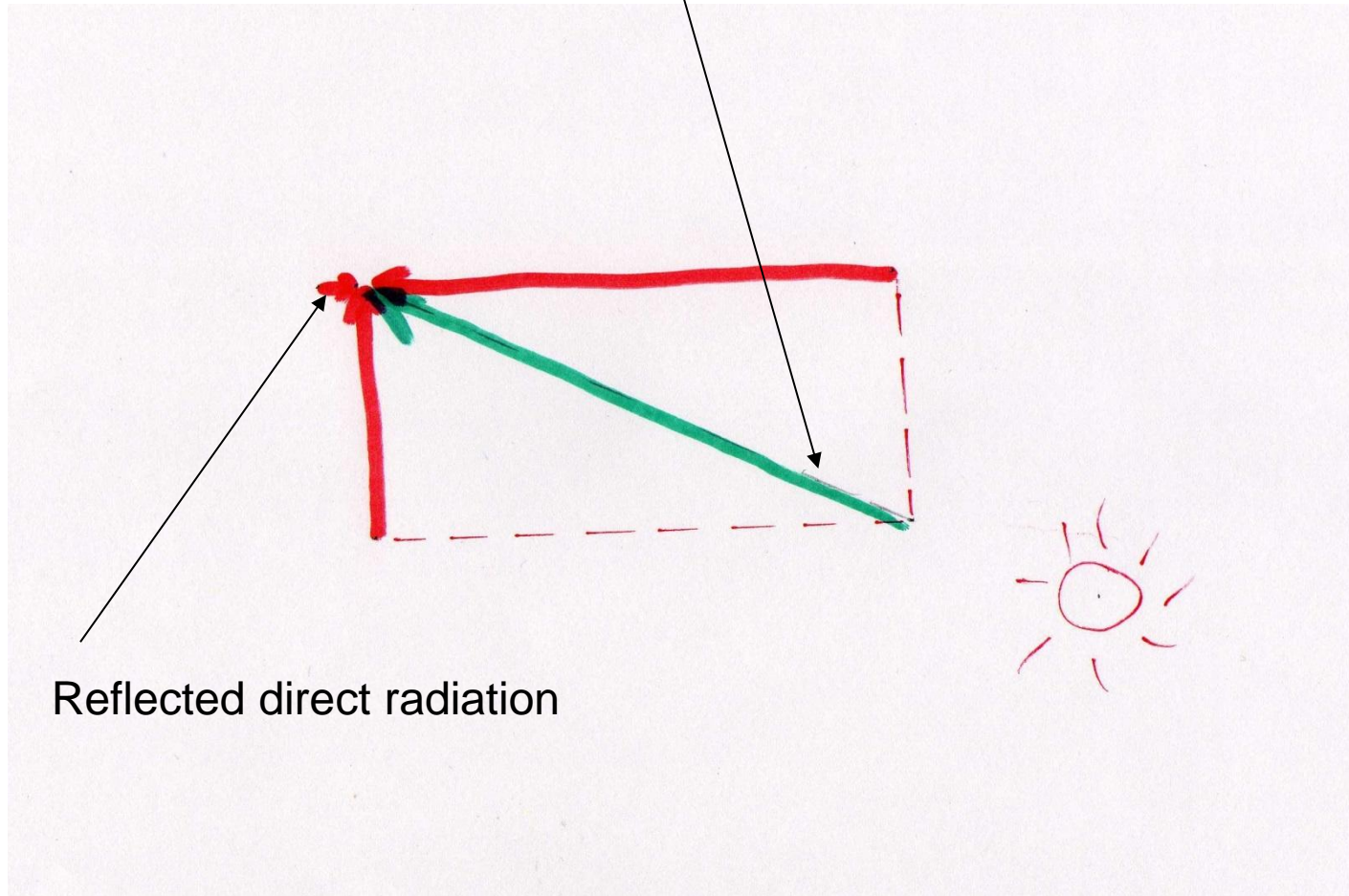


# Horizontal direct radiation



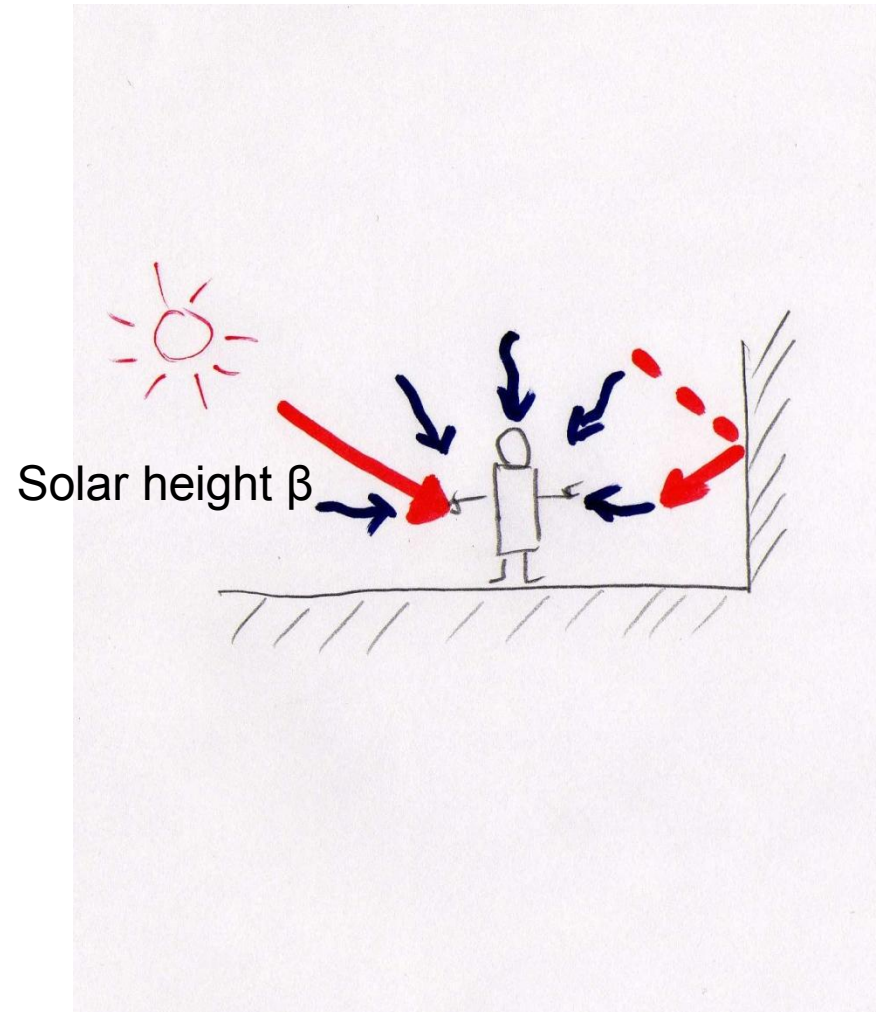
# Resultant horizontal direct radiation

$K_{dir,hor}$

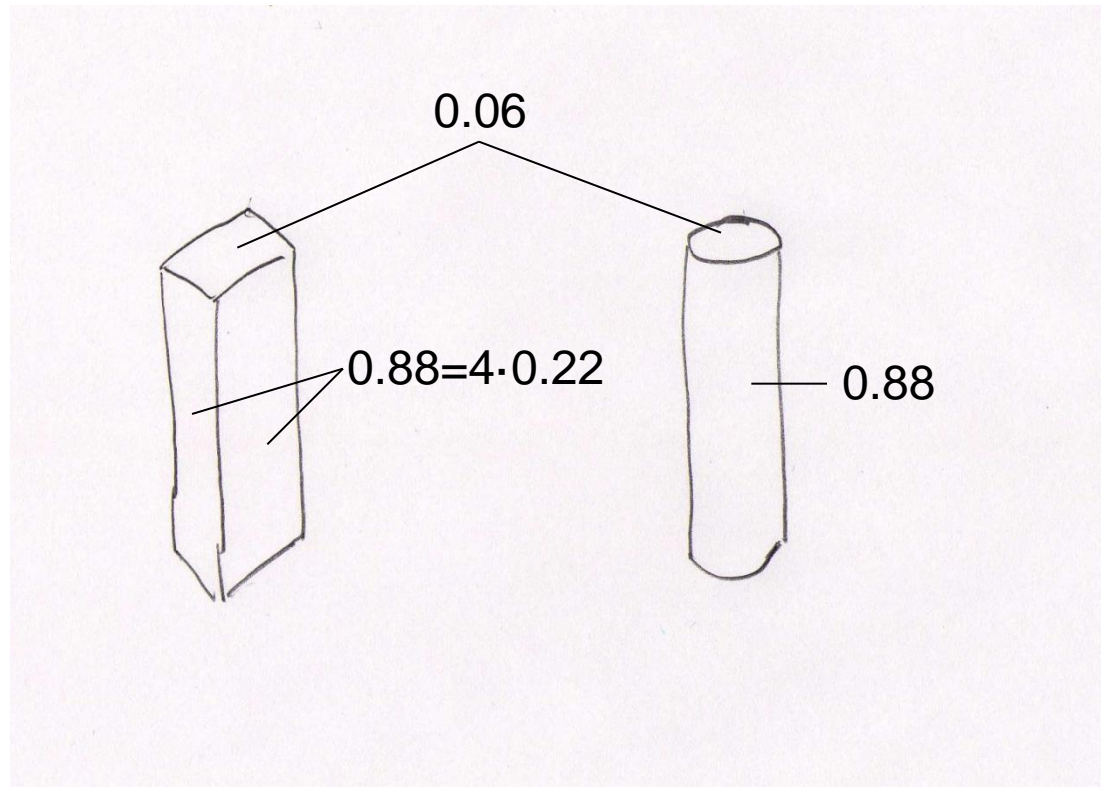


# Direct radiation along the solar rays

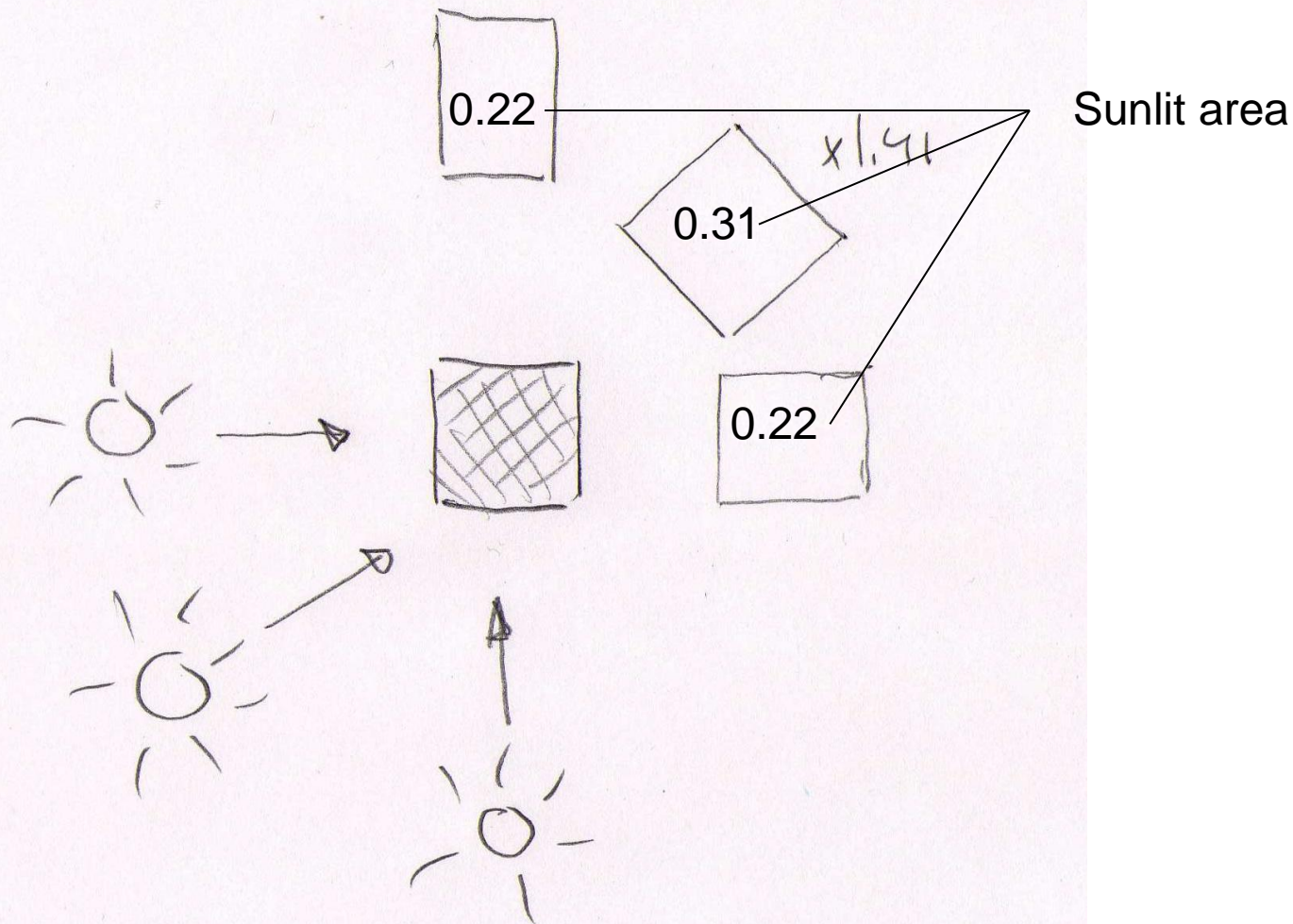
$$K_{\text{dir}} = K_{\text{dir,hor}} \cdot \cos(\beta)$$



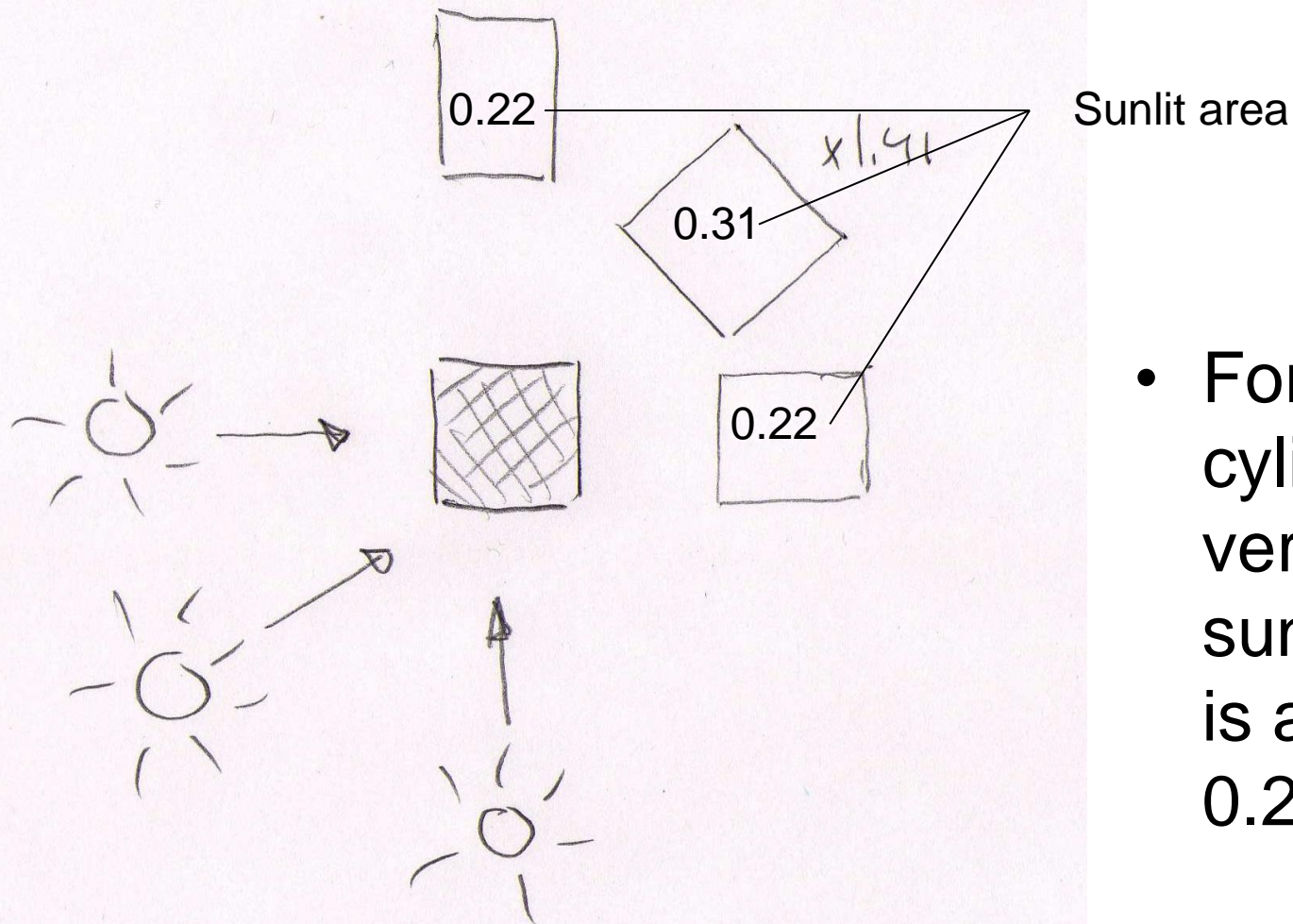
# Proportions of the standing man



# Vertical sunlit area vs azimuth

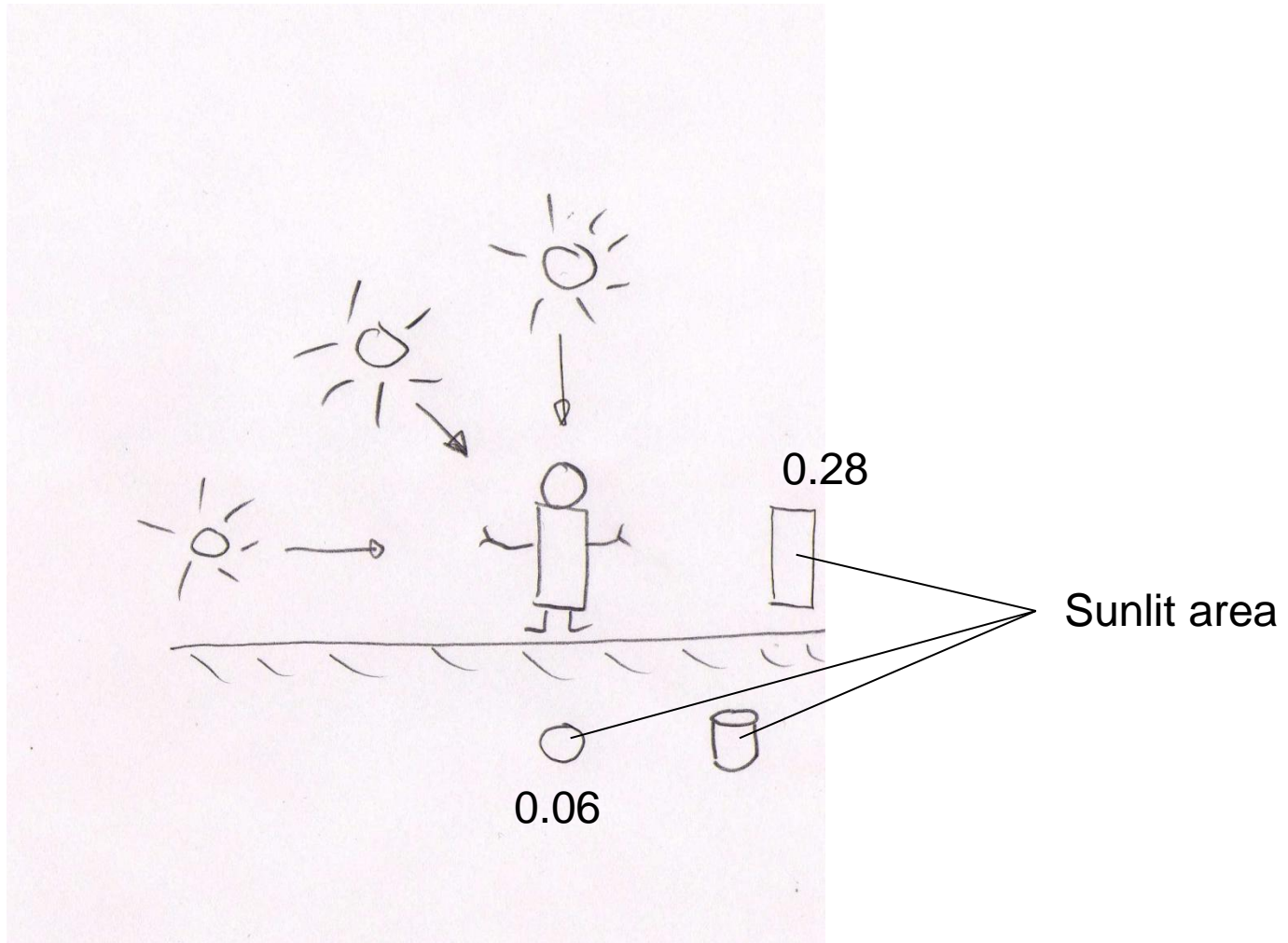


# Vertical sunlit area vs azimuth



- For the cylinder the vertical sunlit area is always 0.28

# Sunlit area vs solar height



# The Höppe calculation (box man)

The mean radiant flux  $S_{\text{str,box}}$ :

$$S_{\text{str,box}} = (1-\alpha) \cdot \underbrace{\sum w_i \cdot K_i}_{\text{shortwave}} + \epsilon \cdot \underbrace{\sum w_i \cdot L_i}_{\text{longwave}}$$

$W_i$  — surface share in direction  $i$

$\alpha$  — albedo

$\epsilon$  — absorbtion coefficient

$$T_{\text{mrt}} = (S_{\text{str,box}} / (\epsilon \cdot \sigma))^{0.25} - 273.15$$

$\sigma$  — Stefan-Boltzmann's constant.

# The new methodology (cylinder man)

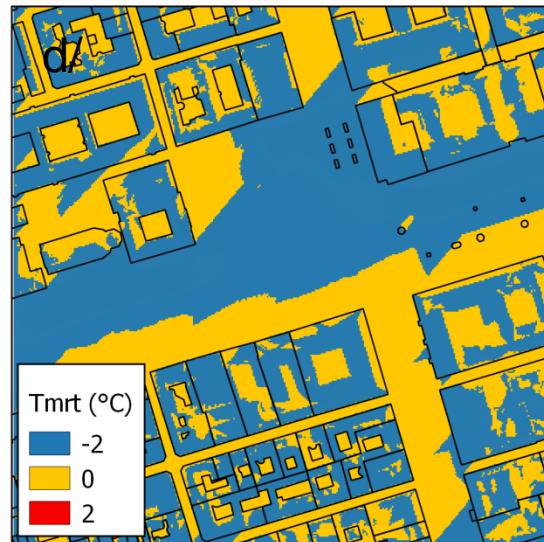
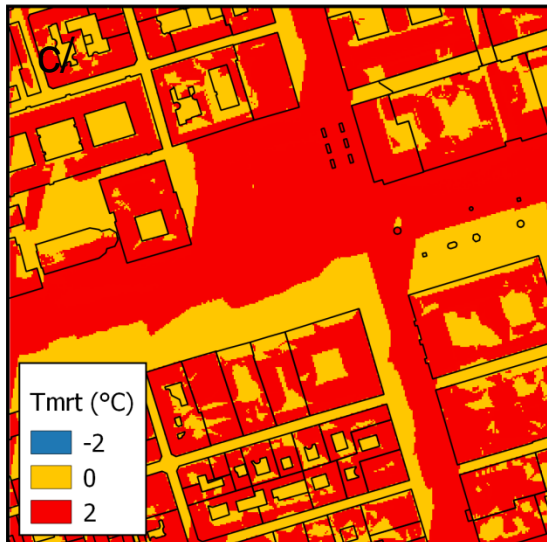
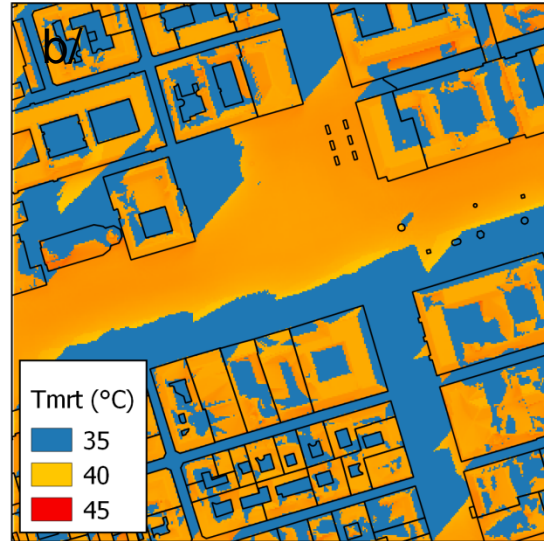
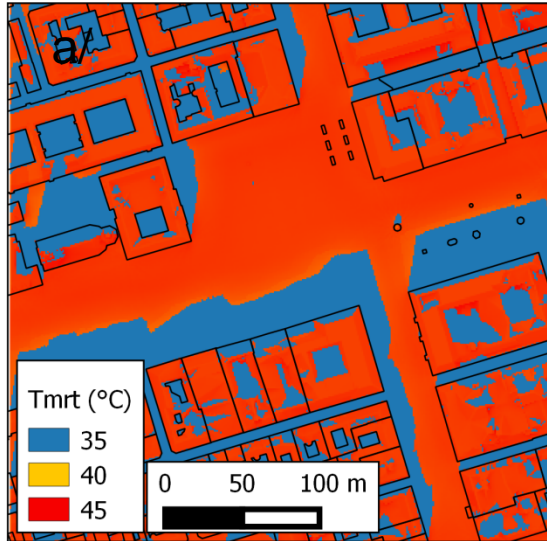
$$S_{\text{str,cyl}} = (1-\alpha) \cdot [0.28 \cdot \cos(\beta) \cdot K_{\text{dir}} + 0.06 \cdot (K_{\uparrow} + K_{\downarrow}) + 0.88 \cdot K_{\text{diff}}] + \varepsilon \cdot \sum w_i \cdot L_i$$

-----  
horizontal direct      vertical global      horizontal diff.      longwave

where  $K_{\text{dir}} = \cos(\beta) \cdot \sqrt{(K_{\text{dir,left}})^2 + (K_{\text{dir,right}})^2}$

# Implementation in models

## - the SOLWEIG model



- Gothenburg on the 11th of October 2005
- a/  $T_{mrt}$  at 1 p.m. according to the cylinder man
- b/  $T_{mrt}$  at 3 p.m. according to the cylinder man
- c/ differences at 1 p.m. in  $T_{mrt}$  between the box man and the cylinder man
- d/ differences at 3 p.m. in  $T_{mrt}$  between the box man and the cylinder man.

# Some remarks

- Two data sets from two different latitudes,  $11^{\circ}\text{N}$  and  $58^{\circ}\text{N}$ , are studied.
- The new calculations show a maximum around noon and an acute distribution during clear skies.
- On overcast days  $T_{\text{mrt}}$  probably differ little from the previous calculations since the direct radiation vanishes.
- At sites with much reflected radiation but the differences between the two methods will probably become smaller than for open sites.

# Some remarks

- A major advantage of the new methodology is that the ambiguities that can be raised around the errors of the hitherto calculations can be put aside and the reliability of the interpretations will increase.

# The globe thermometer

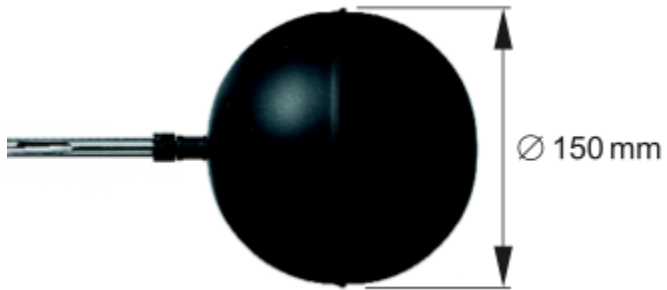
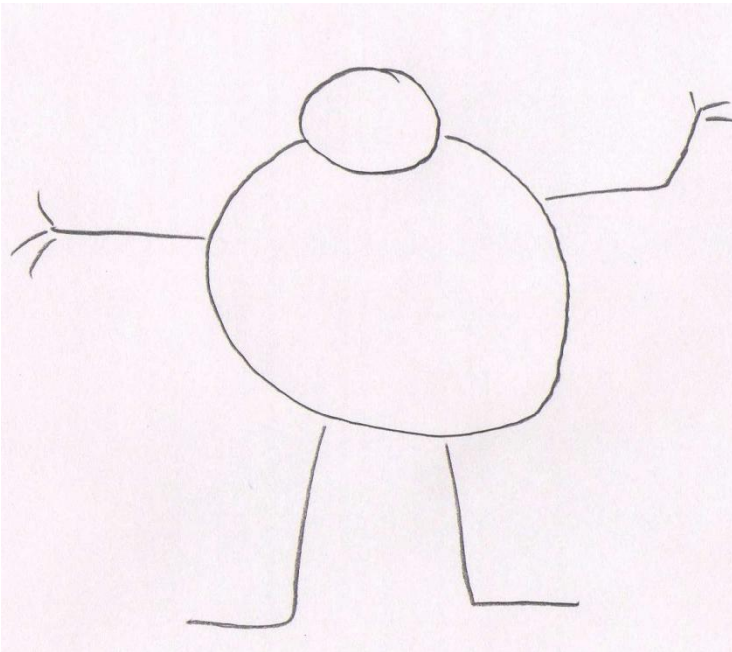


Figure 3. The 38 mm flat grey globe thermometer.

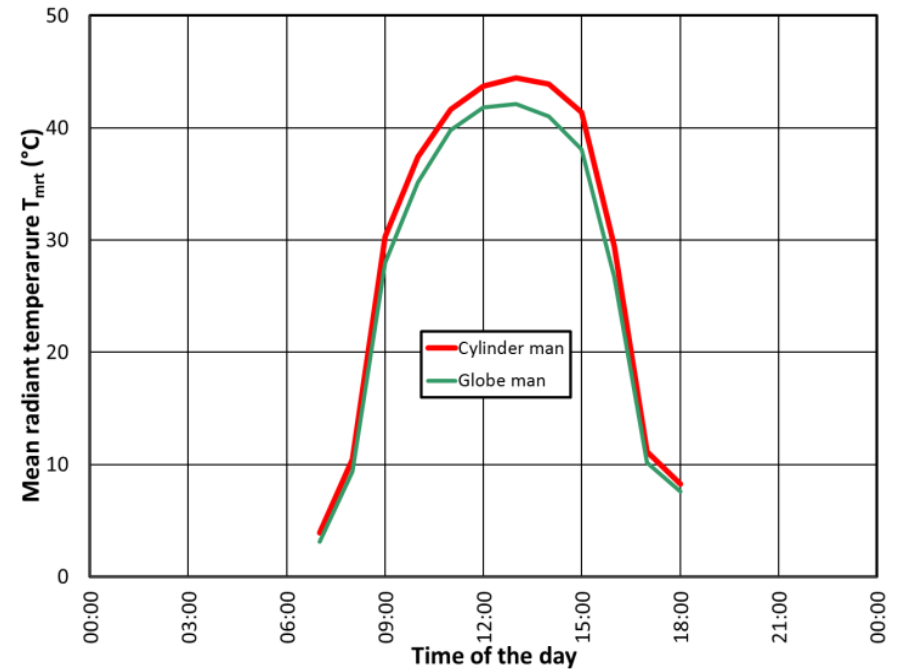
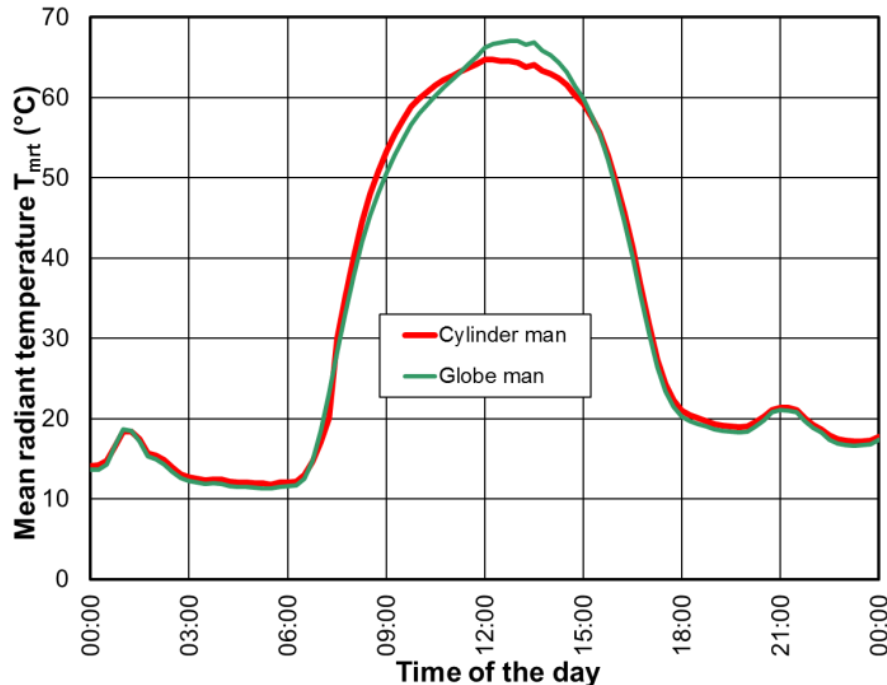
# The globe

$$S_{\text{str,globe}} = (1-\alpha) \cdot [0.25 \cdot K_{\text{dir}} + 1/6 \cdot \sum K_{\text{diff},i}] + \varepsilon \cdot \sum w_i \cdot L_i$$



The surface exposed to the direct radiation is always 0.25

# $T_{mrt}$ calculated with a cylindrical standing man and with a globe.



$T_{mrt}$  in Ouagadougou on the 10<sup>th</sup> of December 2007. Maximum solar elevation 55°.

$T_{mrt}$  in Gothenburg on the 11<sup>th</sup> of October 2005. Maximum solar elevation 30°.

# About the calculations

The calculations are performed in Excel.

This sheet will be available at our homepage. The six directional data had to be complemented with data on solar azimuth and solar height. The sheet includes some steps that were not shown in the presentation, e.g. that the orientation of the radiation equipment is checked and adjusted automatically in the calculation.

# Solweig

The implementation in Solweig is already available.

Get it on our homepage:

[http://gvc.gu.se/english/research/climate/  
urban-climate/software/solweig](http://gvc.gu.se/english/research/climate/urban-climate/software/solweig)

# Thank you for listening

