

An intra-urban nocturnal cooling rate model

ICUC9

Toulouse, France

9th July 2015

Shiho Onomura

Björn Holmer

Fredrik Lindberg

Sofia Thorsson

Urban Climate Group, University of Gothenburg, Sweden



Two-phase nocturnal cooling



Phase 1

- site-dependent
- most intensive cooling
- driven by sensible heat and longwave radiative divergence (Holmer et al. 2007)

Phase 2

- site-independent
- gradually decreasing
- driven by raidative divergence in a capping inversion above the canonpy layer (Holmer et al. 2007)





Objectives

To develop a nocturnal cooling rate model to simulate air temperature investigating the temporal development of nocturnal cooling and the relationship between cooling rates and meteorological variables and building density.



Dataset for model development

- Air temperature (2m) measured at **an open site** and **four built-up sites** with little vegetation in Gothenburg during May-Sep in 1999.
- U (10m), Ta, clearness of the sky (K↓, RH), from a nearby reference station (SMHI).
- Average sky view factor within a 25 m radius calculated using digital surface model and ArcMAP 10.1.

































Phase 1A starts when relative wind speed change drops below -0.2.





Phase 1A starts when relative wind speed change drops below -0.2.

Phase 1B occurs when the atmosphere turns from unstable to stable.

 $t_{\text{peak}} = t_1 + t_2$





Phase 1A starts when relative wind speed change drops below -0.2.

Phase 1B occurs when the atmosphere turns from unstable to stable.

$$\mathbf{t}_{\text{peak}} = \mathbf{t}_1 + \mathbf{t}_2$$

Phase 2 starts 1 hr after relative wind speed change drops below - 0.5.



Determination of CR_{peak}





Determination of CR_{peak}

- clearness of the sky (CI)
- wind speed (U)

- maximum daily air temperature (T_{max})
- sky view factor (SVF)

Cooling rate impact factor (CRIF)

$$CRIF = \left(1 - \frac{U}{U_{crit}}\right) \cdot \frac{(CI - CI_{min})}{(CI_{max} - CI_{min})}$$
$$U_{crit} = 4 \text{ m/s}$$
$$CI_{max} = 1$$
$$CI_{min} = 0.4$$





The relationship between CR_{peak} and T_{max}





The impact of SVF on cooling rate





Determination of CR_{peak}





COTHENEUR Determination of CR₂ $CR_2 = CR_{2_min} + (CR_{2_clear} - CR_{2_min}) \cdot \frac{CI - 0.57}{1 - 0.57}$ $CR_{2_clear} = -1.6 + 0.67 \cdot U_2$ $CR_{2_min} = -0.34 + 0.03 \cdot U_2$ $CR_{2_min} = -0.34 + 0.03 \cdot U_2$

Impact of wind speed change

$$\Delta CR_w(t) = \begin{cases} -\alpha \cdot \left(U(t) - U_{ave,phasex} \right)^{1/3}, & \text{if } x = 1A \\ +\alpha \cdot \left(U(t) - U_{ave,phasex} \right)^{1/3}, & \text{if } x = 1B \text{ or } 2 \end{cases}$$

CI = 1 CI = 0.96

3

2

Wind speed (m s⁻¹) at t_2

1

0

CI = 0.57

4



Fundamental equations

Phase 1A $CR = (CR_1 - CR_{peak}) \cdot (\cos(f(t - t_1)) - 1)/2 + CR_1 + \Delta CR_w(t)$ Phase 1B $CR = (CR_2 - CR_{peak}) \cdot (\cos(f(t - t_{peak})) + 1)/2 + CR_{peak} + \Delta CR_w(t)$

Phase 2 $CR = \frac{t_{end} - t}{t_{end} - t_2} CR_2 + \Delta CR_w(t)$





Model evaluation

Observational data from

- A open (SVF=0.92) site and a built-up (SVF=0.40) site in Gothenburg, Sweden
- A complex built-up (SVF=0.46) site in London, UK
- during May Sep in 2012 and 2014. The sites have little vegetation.











Summary

- A intra-urban nocturnal cooling model was developed based on the concept of two-phase cooling.
- The model successfully estimates cooling rate under a wide range of weather (Cl and U) condition as well as at sites of different building densities.

Future work

- To be tested for other cities, e.g. lower latitudes and/or with very different site characteristics.
- To take into account the impact of anthropogenic heat and latent heat fluxes.
- To be used in climate application, e.g. human thermal comfort estimation.



Thank you for your attention.

Aknowledgement

- This project is financially supported by the Swedish Research Council Formas, the Swedish Energy Agency, the Swedish Environmental Protection Agency, the Swedish National Heritage Board and the Swedish Transport Administration.
- We appreciate Prof. Sue Grimmond, Dr. Simone Kotthaus, Mr. William Morrison and Ms. Janina Konarska for providing observational data.

Relevant research paper

- Onomura S, Homer B, Lindberg F and Thorsson S (2015) Urban nocturnal cooling rates: development and evaluation of the NOCRA Model. Manuscript.
- Konarska J, Homer B, Lindberg F and Thorsson S (2015) Influence of vegetation and building geometry on the spatial variations of air temperature and cooling rates in a high latitude city. In Review, Int J Climatol



Two-phase nocturnal cooling



• Two-phase cooling (ex. Chow and Oke 2006)

Phase 1 : site-dependent most intensive cooling

> Radiative divergence Sensible heat flux

Phase 2 : site-independent gradually decreasing

> Radiative divergence in a capping inversion above the canopy layer



Cooling rate (CR₂) at the start of phase 2





Impact of cloudiness on CR_{peak}





Impact of U and T_{max} on cooling rate















Phase 1 starts when relative wind speed change drops below -0.2.

Most intensive cooling occurs when the atmosphere turns from unstable to stable.

$$t_{\text{peak}} = (t_1 + t_2)/2$$







Phase 1 starts when relative wind speed change drops below -0.2.

Most intensive cooling occurs when the atmosphere turns from unstable to stable.

Phase 2 starts about 1 hour after relative wind speed change drops below -0.5.



built-up