



# CFD Modeling of Reactive Pollutants in an Urban Street Canyon using Different Chemical Mechanisms

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# Introduction

- ❖ At microscale the atmosphere and urban distributions interaction generates a complex flow and heterogeneous dispersion of pollutants within the canopy
- ❖ An accurate understanding of Urban Air Quality requires considering a coupled behavior between dispersion of reactive pollutants and atmospheric dynamics
- ❖ Urban Air Pollution → Traffic emissions



- Nitrogen Oxide (NO)
- Nitrogen dioxide (NO<sub>2</sub>)
- Volatile Organic Compounds (VOCs)

# Limitations

- ❖ In a real and complex geometry, the required computational time is large
- ❖ Implementing chemical reactions in a CFD model increase the CPU time considerably due to the coupling of pollutant transport equations



# Objectives

To simulate the pollutants dispersion considering chemistry:

- ❖ To reproduce reactive pollutant distribution using the simplest chemical mechanism minimizing CPU time
- ❖ Analyze the conditions in which the implementation of a complex chemical mechanism is necessary

# Structure

To model in 2D and 3D idealized urban geometries:

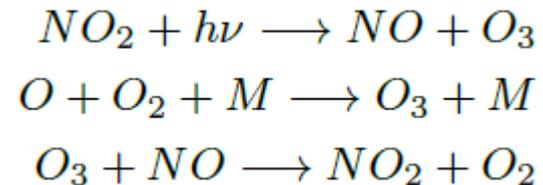
- ❖ The chemical and dynamic coupling under different chemical approaches:
  - (a)** Passive tracer (non-reactive)
  - (b)** NO<sub>x</sub>-O<sub>3</sub> photostationary state (PSS)
  - (c)** Complex chemical mechanism (CCM)
- ❖ Evaluation of the influence of atmospheric parameters (wind speed and ozone concentration)

Quantify the variation on NO and NO<sub>2</sub> concentration with the use of chemical mechanism

# Chemical Mechanisms

**Passive Tracer** → Considering NO and NO<sub>2</sub> non-reactive

**Photostationary State** →



**Complex Chemical Mechanism** → 23 chemical species  
25 chemical reactions

Due to the limitation of CPU time, CCM has been reduced based on Regional Atmospheric Chemistry Mechanism (RACM) using CHEMATA program software (Kirchner, 2005)

# Study scenarios

**Ozone**

**Geometry**

**Wind Speed**

$$O_3 = 10 \text{ ppb}$$

$$O_3 = 40 \text{ ppb}$$

2D

3D

$$u(z = 2H) = 2 \text{ m s}^{-1}$$

$$u(z = 2H) = 4 \text{ m s}^{-1}$$

- Passive tracer (non-reactive)
- NO<sub>x</sub>-O<sub>3</sub> photostationary state (PSS)
- Complex chemical mechanism (CCM) →

Different ratios of VOCs-to-NO<sub>x</sub> emission:

$$\text{VOCs/NO}_x = 1/5$$

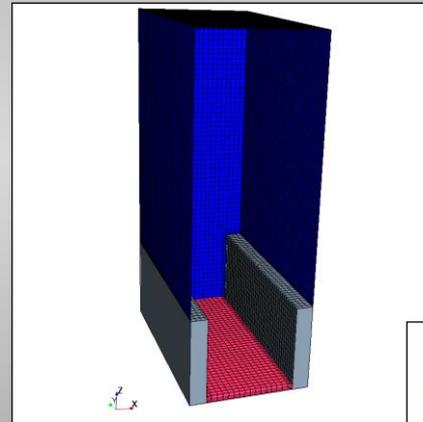
$$\text{VOCs/NO}_x = 1/2$$

# CFD Model description

- ❖ Reynolds-averaged Navier-Stokes (RANS) equations with a  $k-\epsilon$  turbulence model
- ❖ Transport equations of chemical species

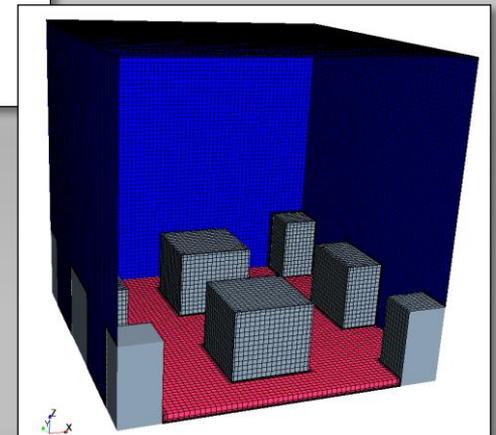
$$\frac{\partial C_i}{\partial t} + U_i \frac{\partial C_i}{\partial x_j} = D \frac{\partial^2 C_i}{\partial x_j \partial x_j} + \frac{\partial}{\partial x_j} \left( K_c \frac{\partial C_i}{\partial x_j} \right) + [\Delta C_i]_{Chem} + S_{C_i}$$

- ❖ Computational domains
  - 2D-geometry: Street-Canyon
    - 24x40x64 m



3D-geometry: Staggered Array of cubes:

- 64x64x64 m
- $\lambda_p = 0.25$



# Simulation Set up

## ❖ Boundary conditions for momentum equations

- Simulating an infinite number of streets

y-direction → zero gradient boundary conditions

x-direction → Periodic Conditions:

$$\frac{\partial P}{\partial x} = \rho u_{\tau}^2 / 4H$$

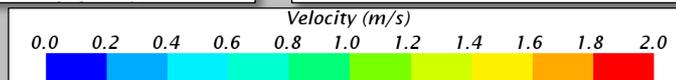
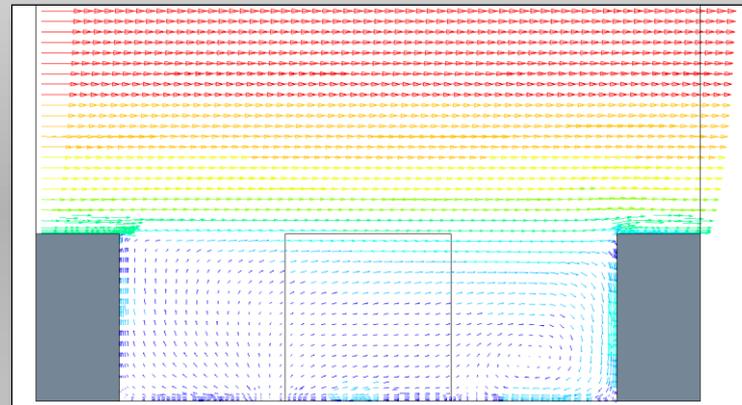
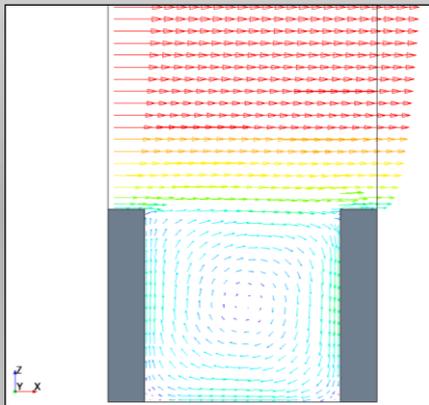
$u_{\tau}$ : Reference velocity  
H: Buildings height

$$u_{\tau} = 0.45 \text{ m s}^{-1}$$

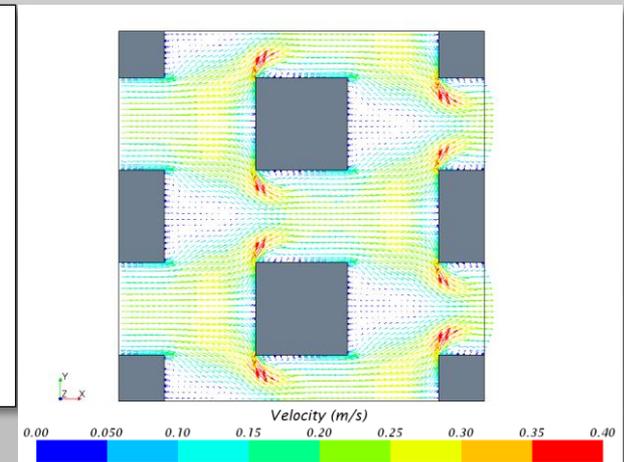
$$u_{\tau} = 0.225 \text{ m s}^{-1}$$

## Flow field:

### 2D-Geometry



### 3D-Geometry

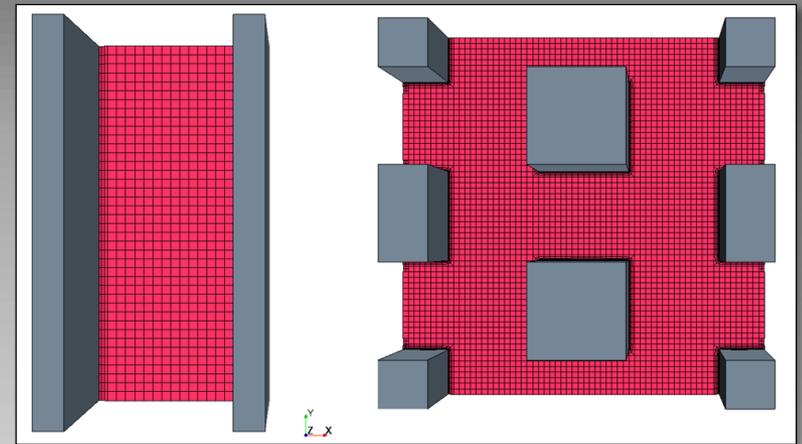


# Simulation Set up

## ❖ Traffic Emissions

- Located at the bottom
- NOx fixed emissions:

$$\left\{ \begin{array}{l} S_{\text{NO}} = 112 \mu\text{g m}^{-1}\text{s}^{-1} \\ S_{\text{NO}_2} = 17 \mu\text{g m}^{-1}\text{s}^{-1} \end{array} \right. \longrightarrow \text{For all emissions cases}$$



- VOCs emissions  $\longrightarrow$  Complex Chemical Mechanism

- VOCs-to-NOx emissions :  $\left\{ \begin{array}{l} \text{VOCs/NO}_x = 1/5 \quad (\text{CCM5}) \\ \text{VOCs/NO}_x = 1/2 \quad (\text{CCM2}) \end{array} \right.$

# Simulation Set up

## ❖ Top Conditions

- Constant concentration at the top →

Important role within the canyon

<b>NO</b>	16 ppb
<b>NO2</b>	35 ppb

- VOCs concentration at the top change with emission ratio
- $[O_3]$  is computed using photostationary equilibrium and is dependent on zenith angle ( $\theta$ )

$$\theta = 45^\circ$$

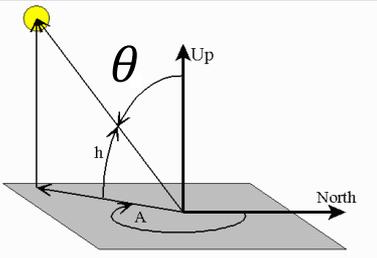
$$\theta = 78^\circ$$

$$J_{NO_2} = A \exp(B/\cos(\theta)) \quad (A \text{ and } B \text{ are constant})$$

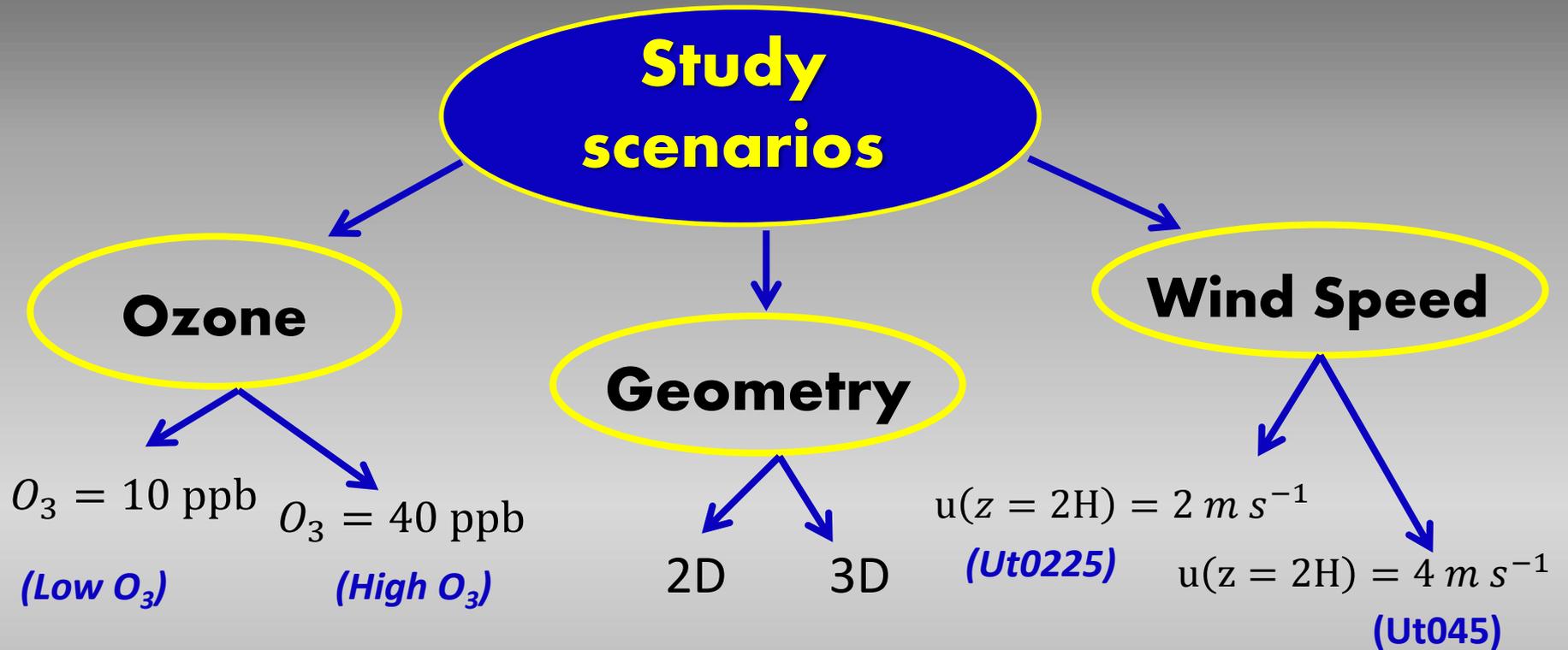
$$[O_3] = \frac{J_{NO_2} [NO_2]}{k [NO]}$$

$$O_3 = 40 \text{ ppb}$$

$$O_3 = 10 \text{ ppb}$$



# Evaluation of Atmospheric Parameters



- Passive tracer (non-reactive) (*P*)
- NO<sub>x</sub>-O<sub>3</sub> photostationary state (*PSS*)
- Complex chemical mechanism (CCM) →

VOCs-to-NO<sub>x</sub> emission

VOCs/NO<sub>x</sub>=1/5 (*CCM5*)

VOCs/NO<sub>x</sub>=1/2 (*CCM2*)

# Evaluation of Atmospheric Parameters

- ❖ In order to compare the scenarios, the concentration is normalized:

$$C_{norm} = \frac{C u_{\tau} W}{Q} \quad (\text{Street Canyon})$$

$$C_{norm} = \frac{C u_{\tau} A_{Em}^2}{Q} \quad (\text{Staggered Array of cubes})$$

W: Street width

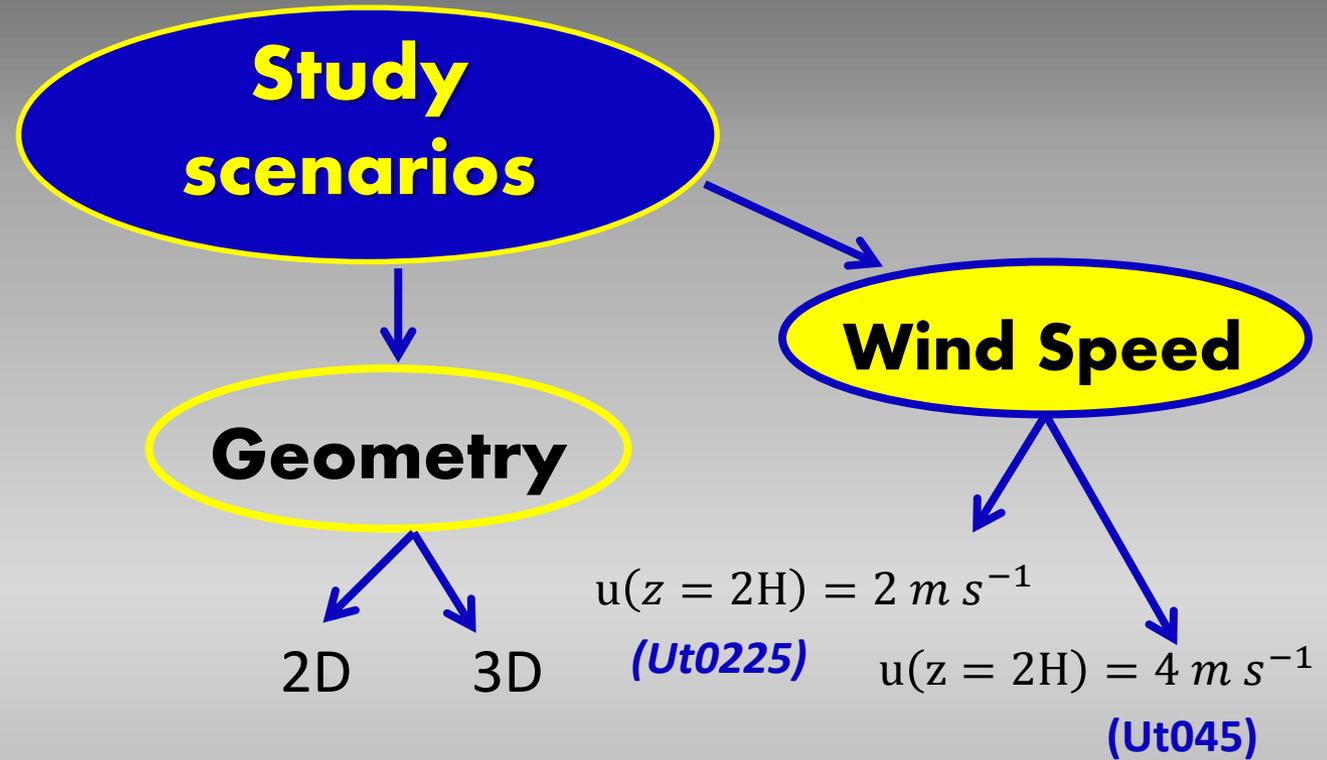
L: Street length

Q: Source emission rate ( $\mu g m^{-1} s^{-1}$ )

- ❖ The difference with respect to Passive tracer is quantify using:

$$\delta C (\%) = \frac{C_{norm} - C_{norm}(P)}{C_{norm}(P)} \times 100$$

# Evaluation of Atmospheric Parameters



- Passive tracer (non-reactive) (*P*)
- NO<sub>x</sub>-O<sub>3</sub> photostationary state (*PSS*)
- Complex chemical mechanism (CCM) →

VOCs-to-NO<sub>x</sub> emission

VOCs/NO<sub>x</sub>=1/5 (*CCM5*)

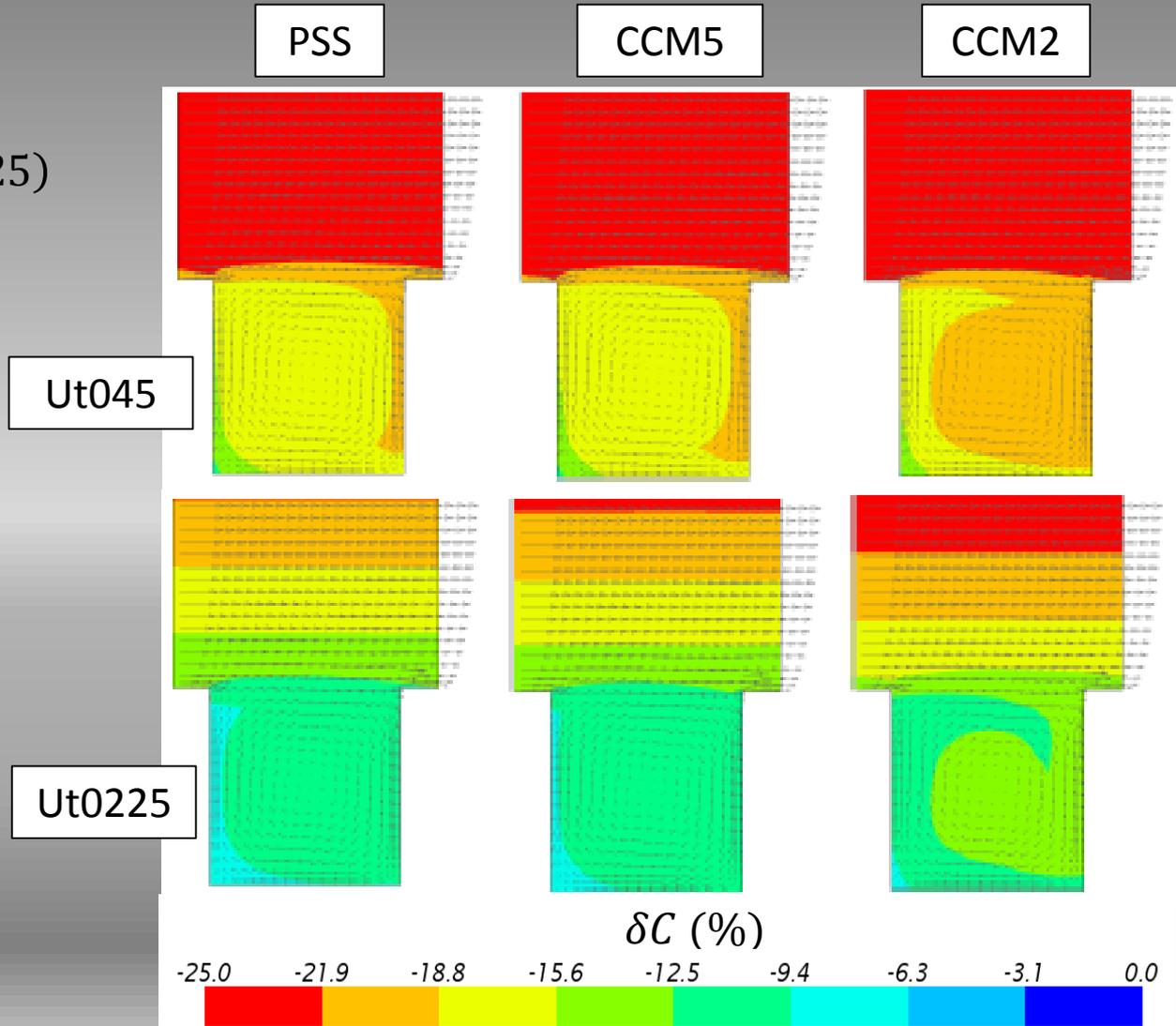
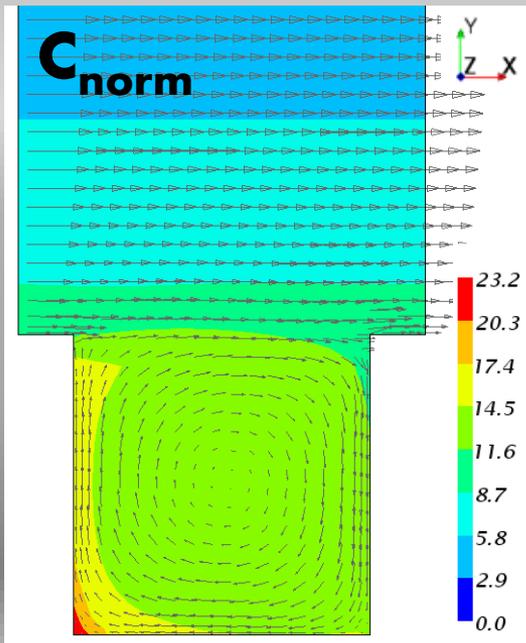
VOCs/NO<sub>x</sub>=1/2 (*CCM2*)

# Wind Speed

$\delta[\text{NO}]$

- $\delta C(\text{Ut045}) > \delta C(\text{Ut0225})$
- Bigger differences with higher VOCs emissions

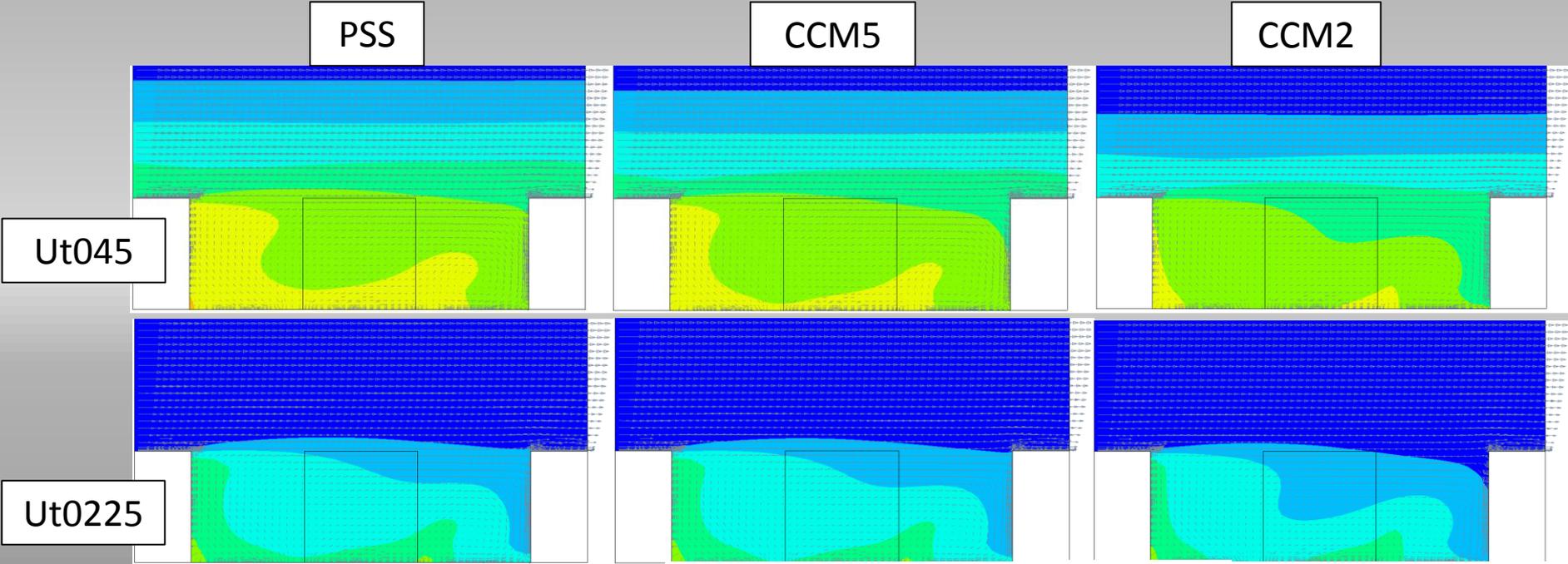
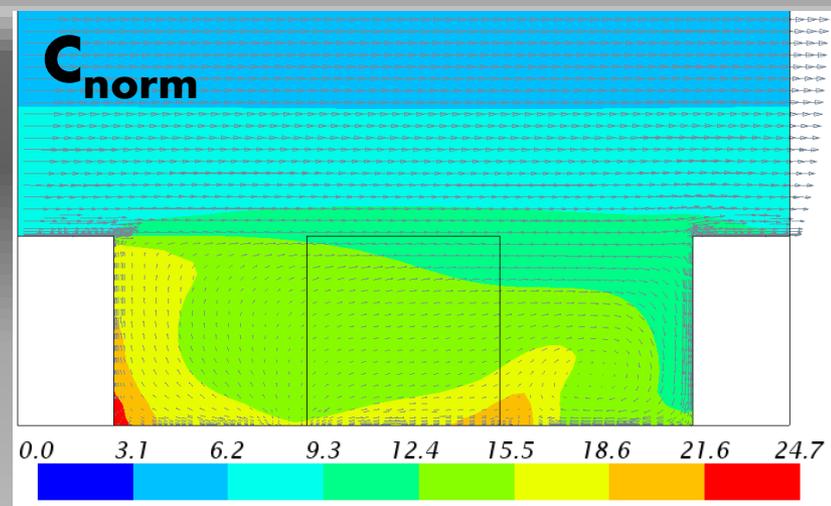
$$\delta C (\%) = \frac{C_{\text{norm}} - C_{\text{norm}}(P)}{C_{\text{norm}}(P)} \times 100$$



# Wind Speed

$\delta[\text{NO}]$

- More ventilation implies less differences between chemical mechanisms



$$\delta C (\%) = \frac{C_{norm} - C_{norm}(P)}{C_{norm}(P)} \times 100$$

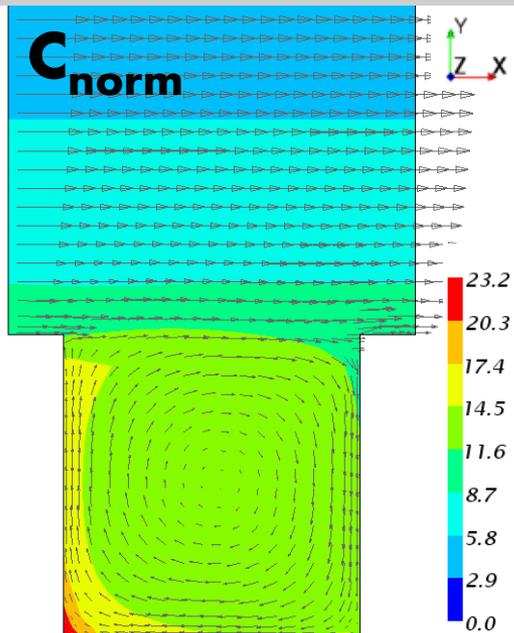


# Wind Speed

$$\delta C (\%) = \frac{C_{norm} - C_{norm}(P)}{C_{norm}(P)} \times 100$$

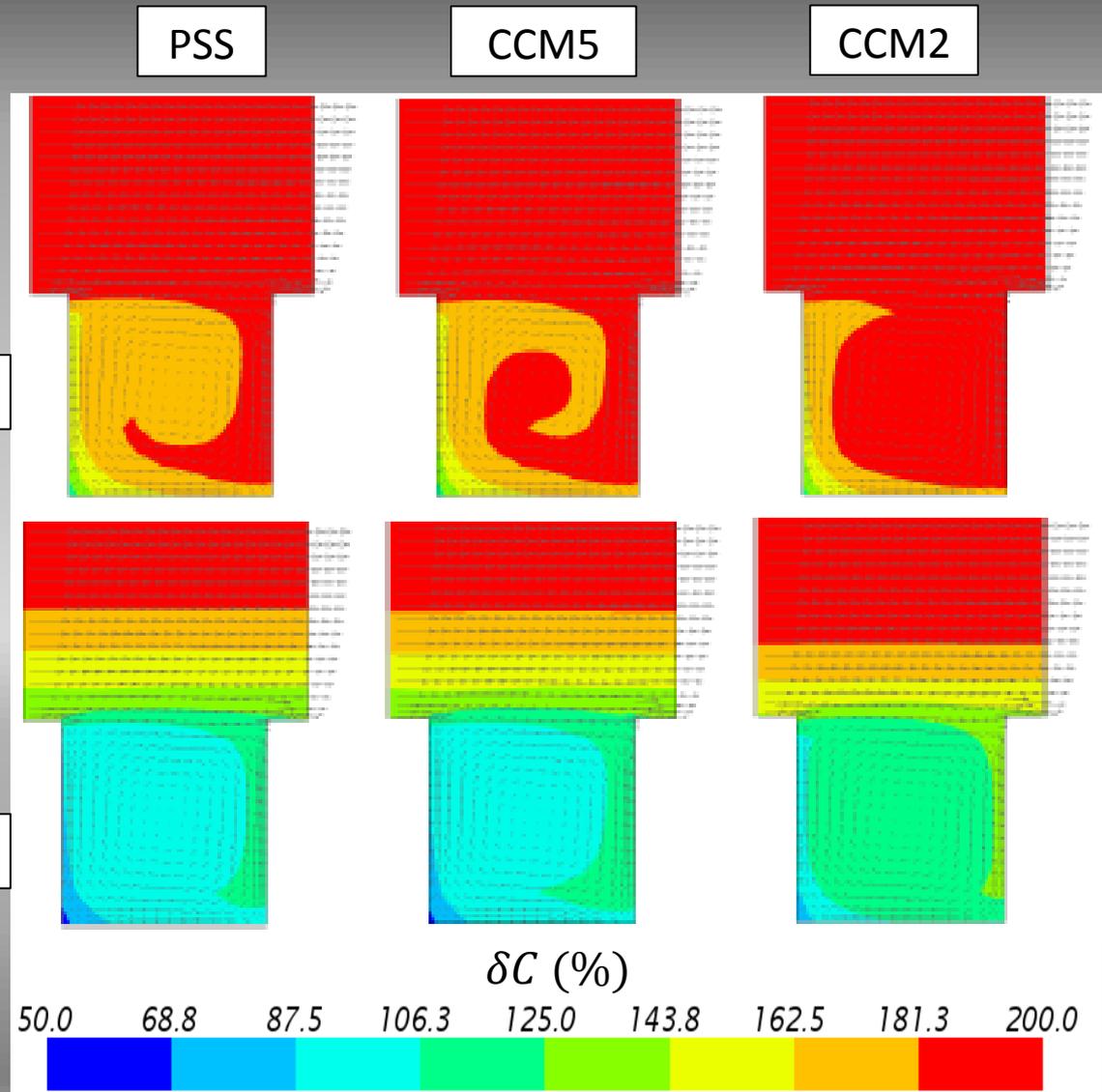
$\delta[\text{NO}_2]$

- $\delta C (Ut045) > \delta C (Ut0225)$
- Differences between all chemical systems



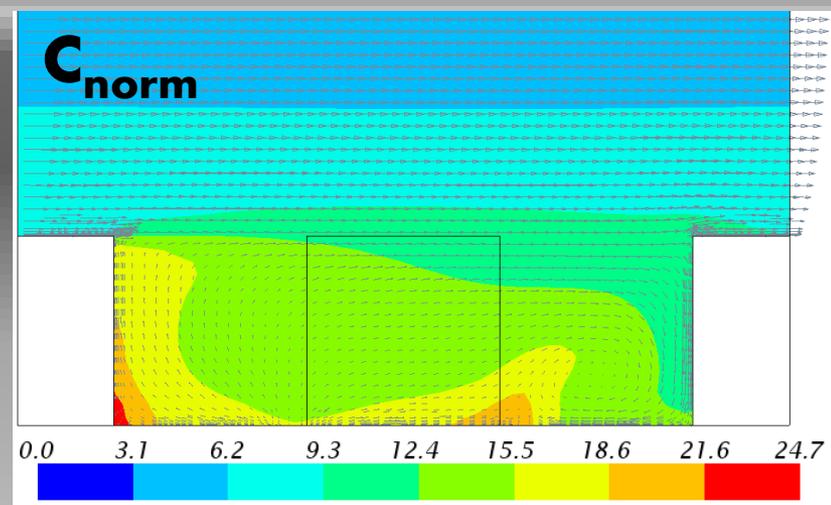
Ut045

Ut0225



# Wind Speed

$\delta[\text{NO}_2]$



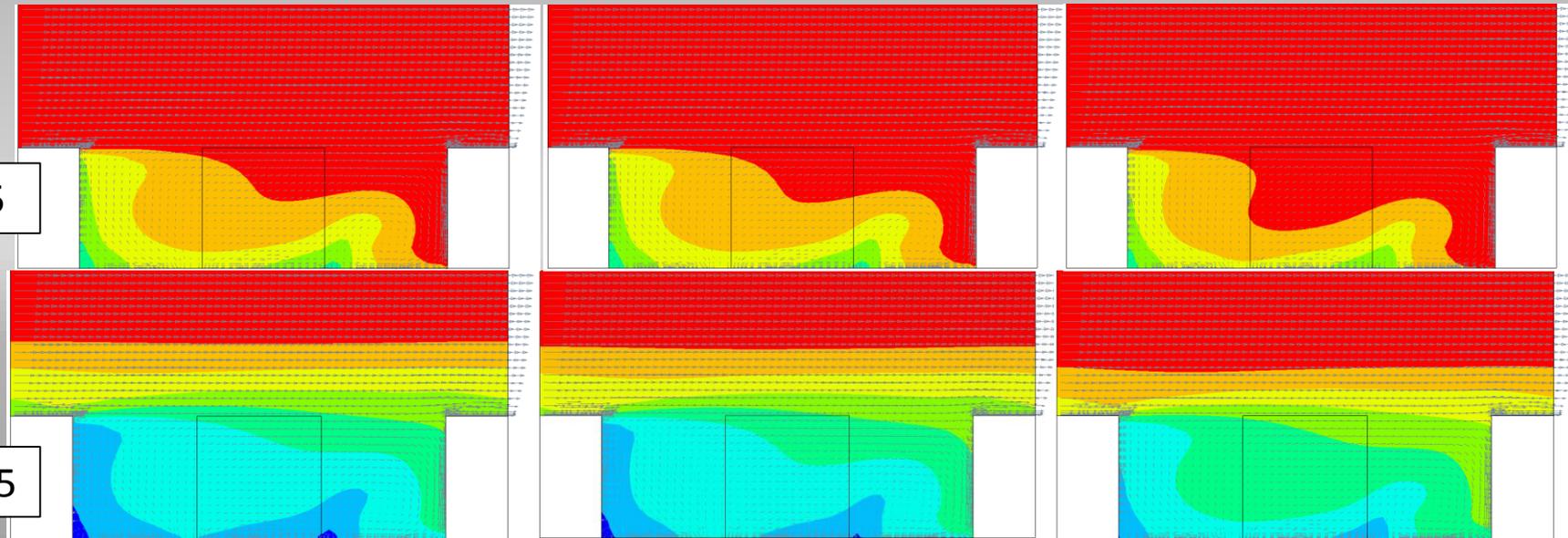
PSS

CCM5

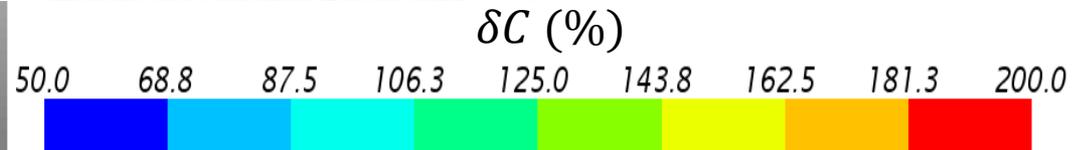
CCM2

Ut045

Ut0225



$$\delta C (\%) = \frac{C_{norm} - C_{norm}(P)}{C_{norm}(P)} \times 100$$



# Wind Speed

## Vertical profiles

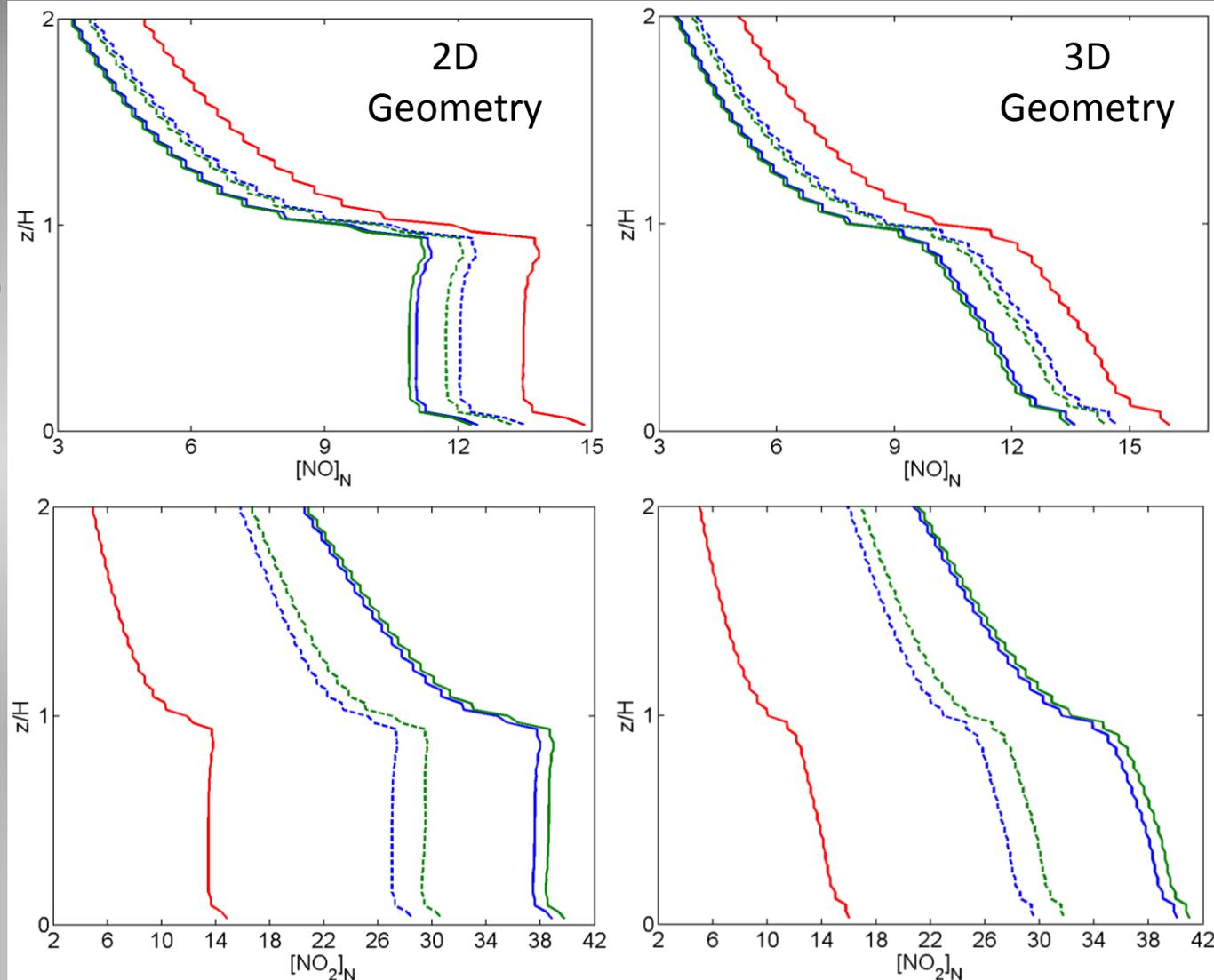
$$C_{norm} = \frac{C u_{\tau} W}{Q}$$

$$C_{norm} = \frac{C u_{\tau} A^2_{Em}}{Q}$$

- Horizontal spatial averaged of  $[NO]_N$  and  $[NO_2]_N$

$\delta C(Ut045) > \delta C(Ut0225)$

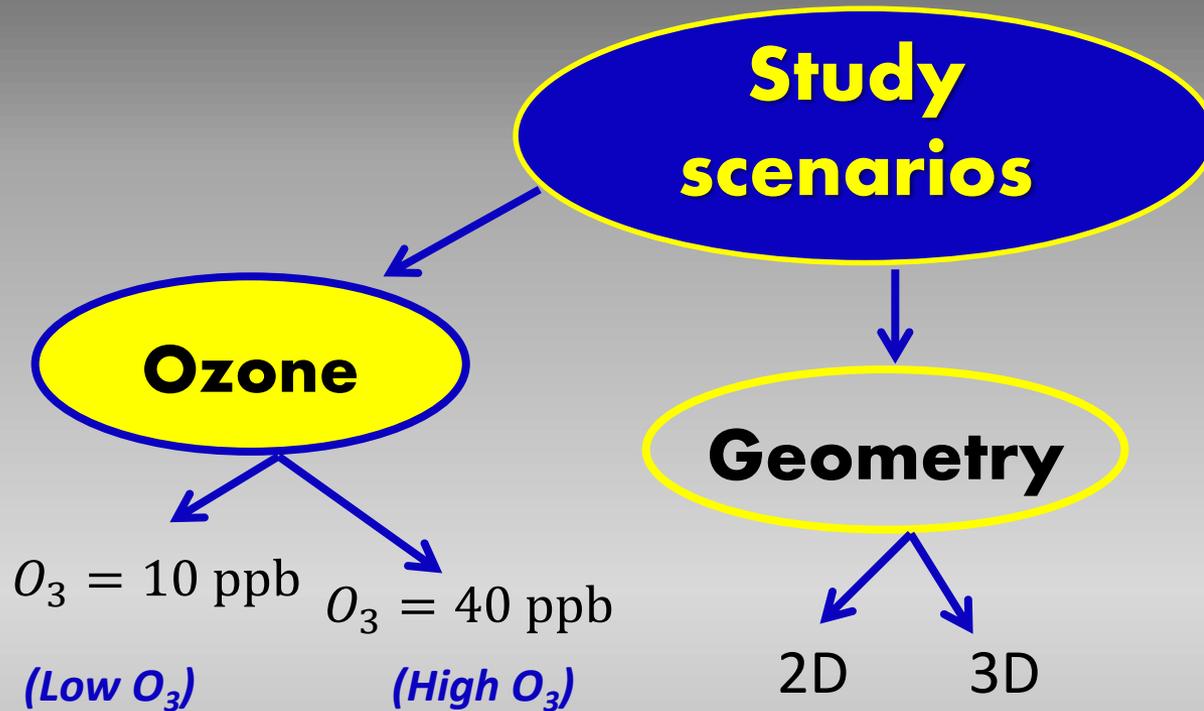
- Lower velocity implies more differences between chemical systems



(solid line): Ut045  
(dashed line): Ut0225

- Tracer
- PSS
- CCM (VOCs/ $NO_x = 1/2$ )
- PSS
- CCM (VOCs/ $NO_x = 1/2$ )

# Evaluation of Atmospheric Parameters



- Passive tracer (non-reactive) (*P*)
- NO<sub>x</sub>-O<sub>3</sub> photostationary state (*PSS*)
- Complex chemical mechanism (CCM) →

VOCs-to-NO<sub>x</sub> emission

VOCs/NO<sub>x</sub>=1/5 (*CCM5*)

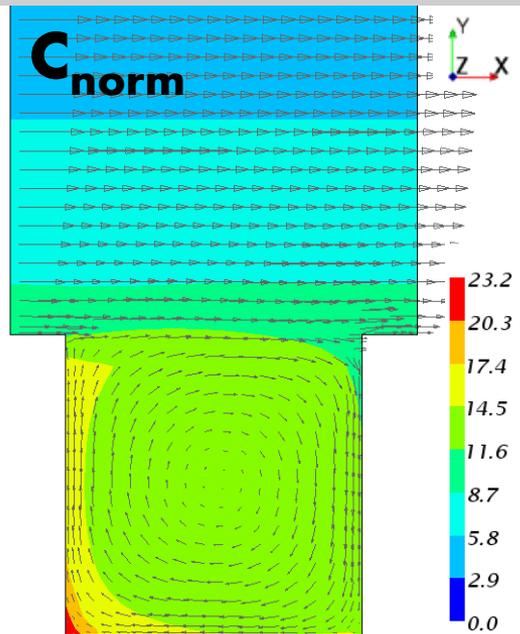
VOCs/NO<sub>x</sub>=1/2 (*CCM2*)

# Ozone

$\delta[\text{NO}]$

- $\delta C$  (High  $O_3$ ) >  $\delta C$  (Low  $O_3$ )
- Differences between all chemical systems with high  $O_3$

$$\delta C (\%) = \frac{C_{\text{norm}} - C_{\text{norm}}(P)}{C_{\text{norm}}(P)} \times 100$$



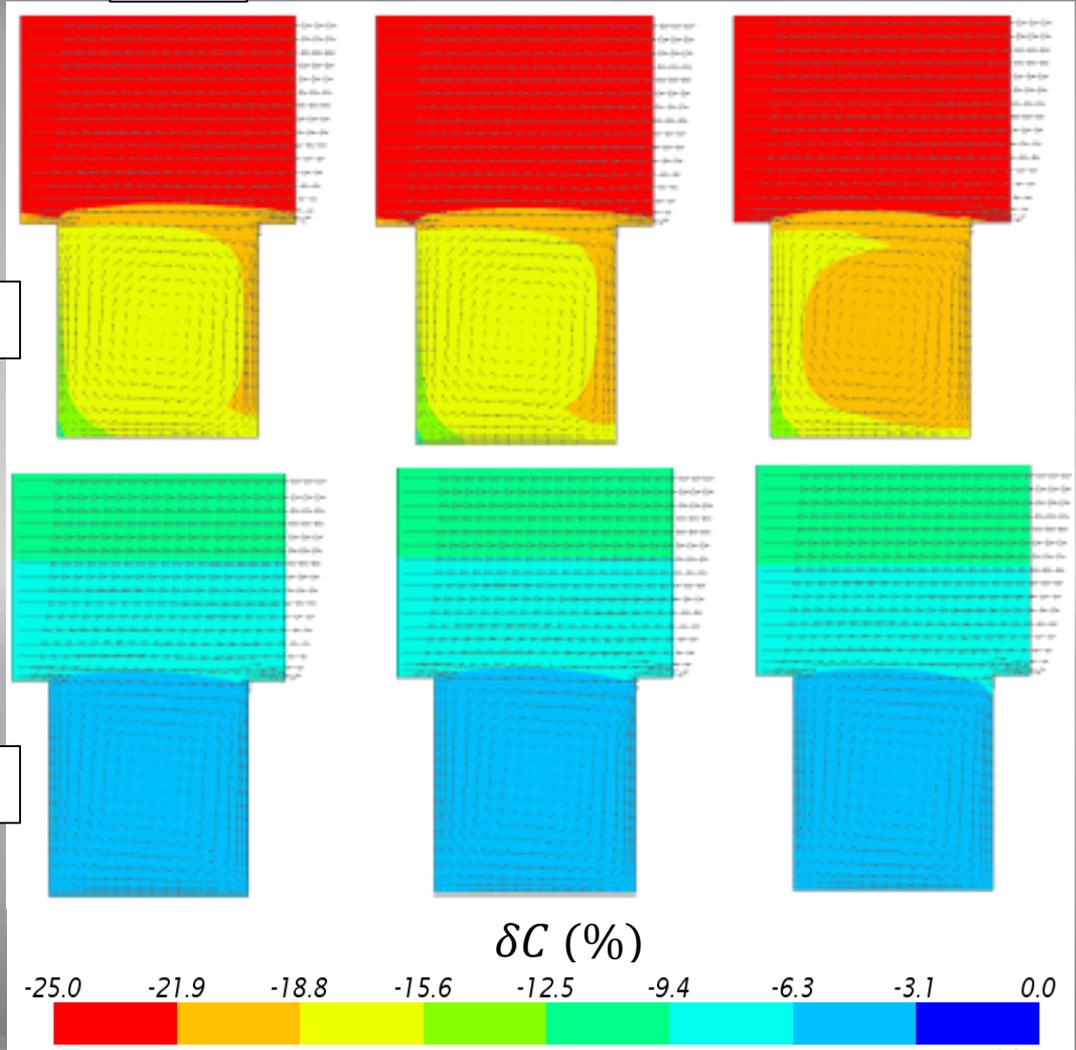
High  $O_3$

Low  $O_3$

PSS

CCM5

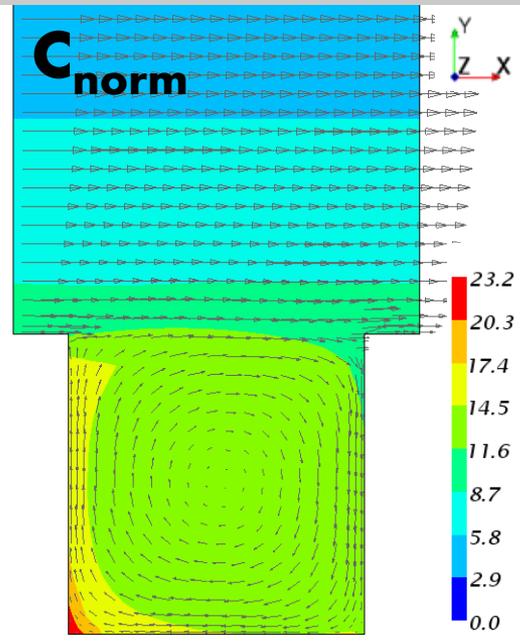
CCM2



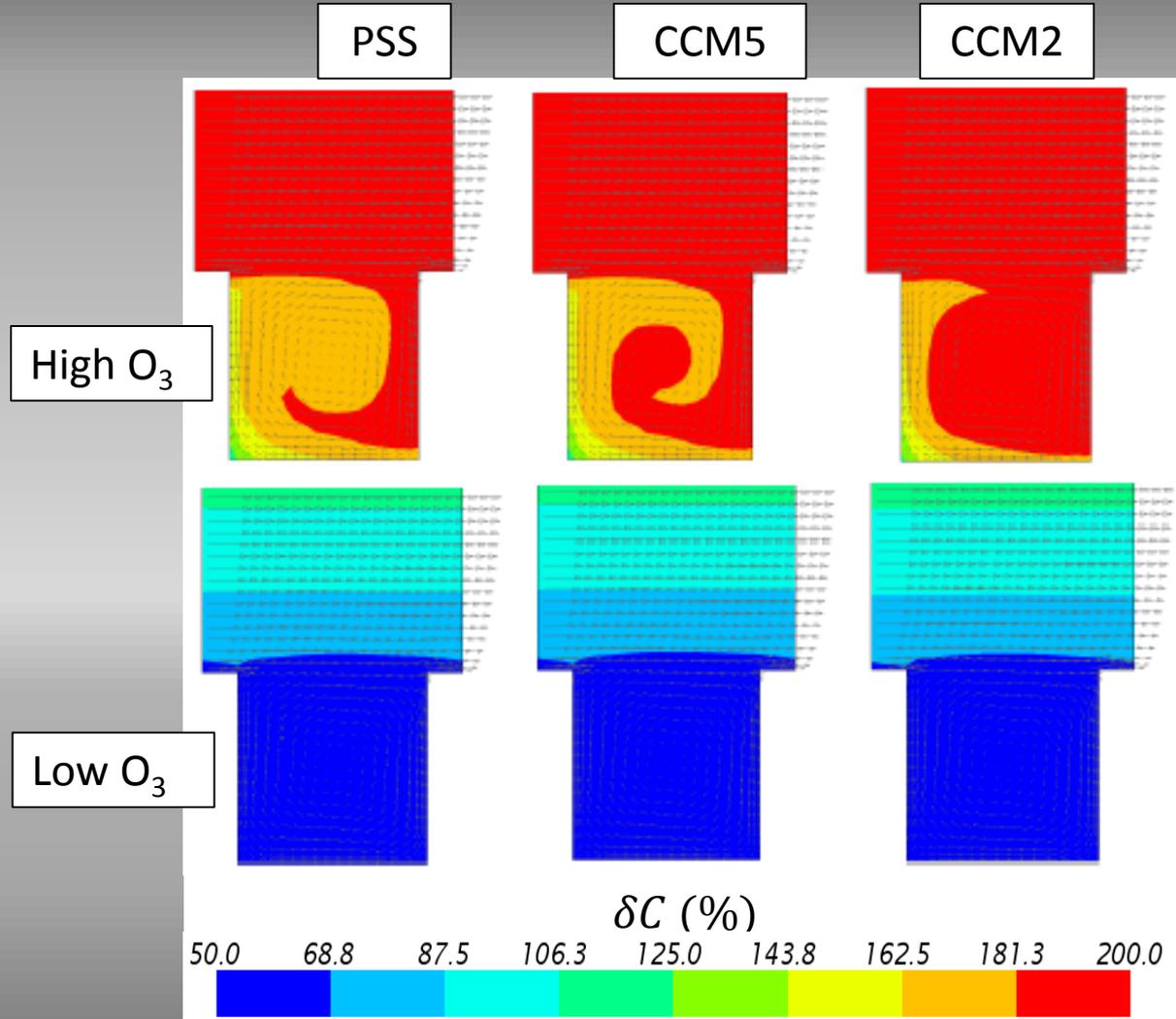
# Ozone

$\delta[\text{NO}_2]$

- $\delta C$  (High  $O_3$ ) >  $\delta C$  (Low  $O_3$ )
- Differences between all chemical systems with high  $O_3$



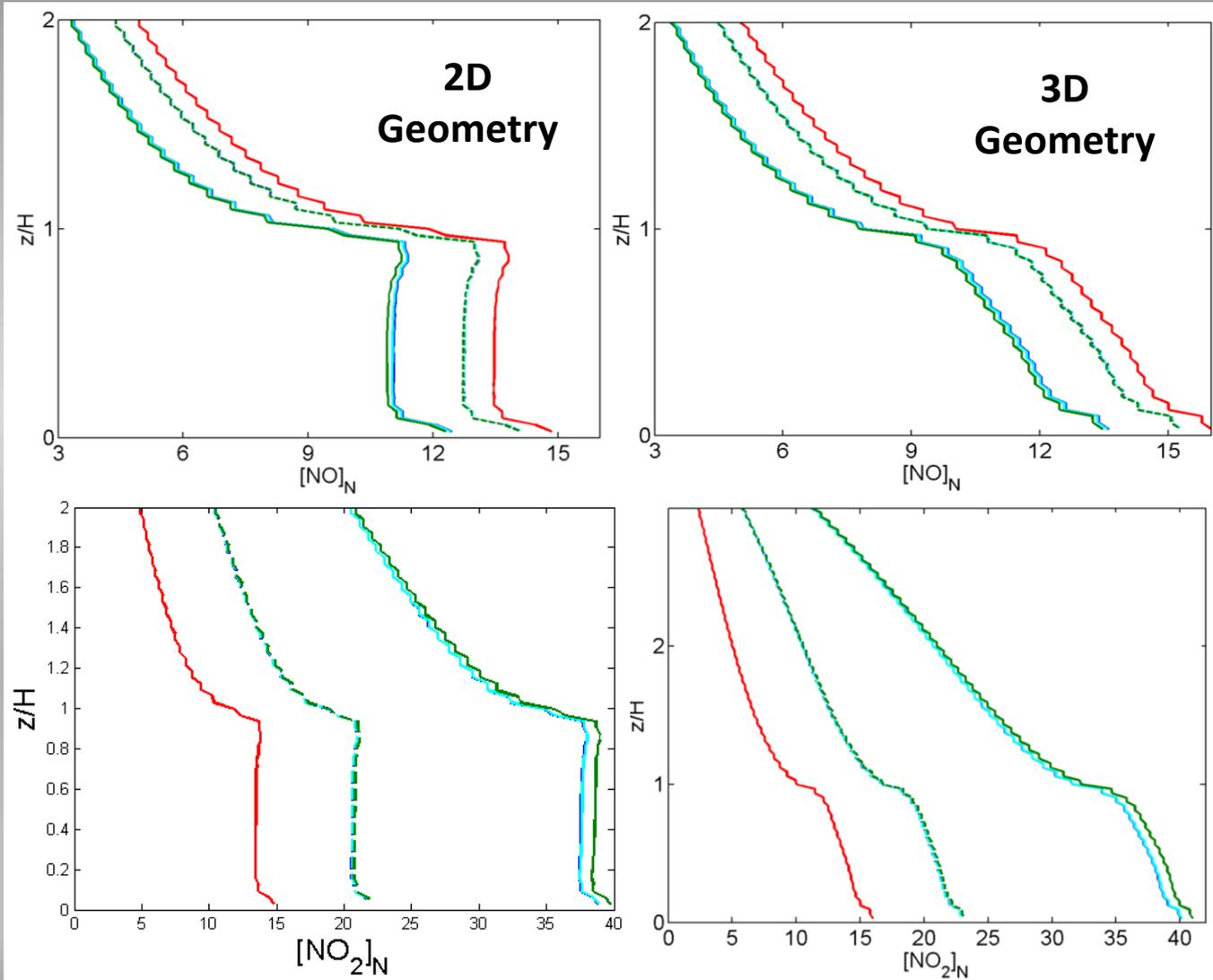
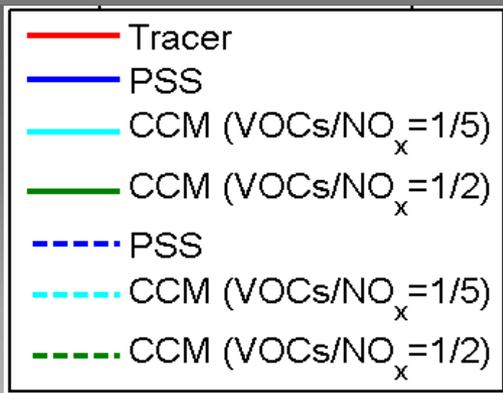
$$\delta C (\%) = \frac{C_{norm} - C_{norm}(P)}{C_{norm}(P)} \times 100$$



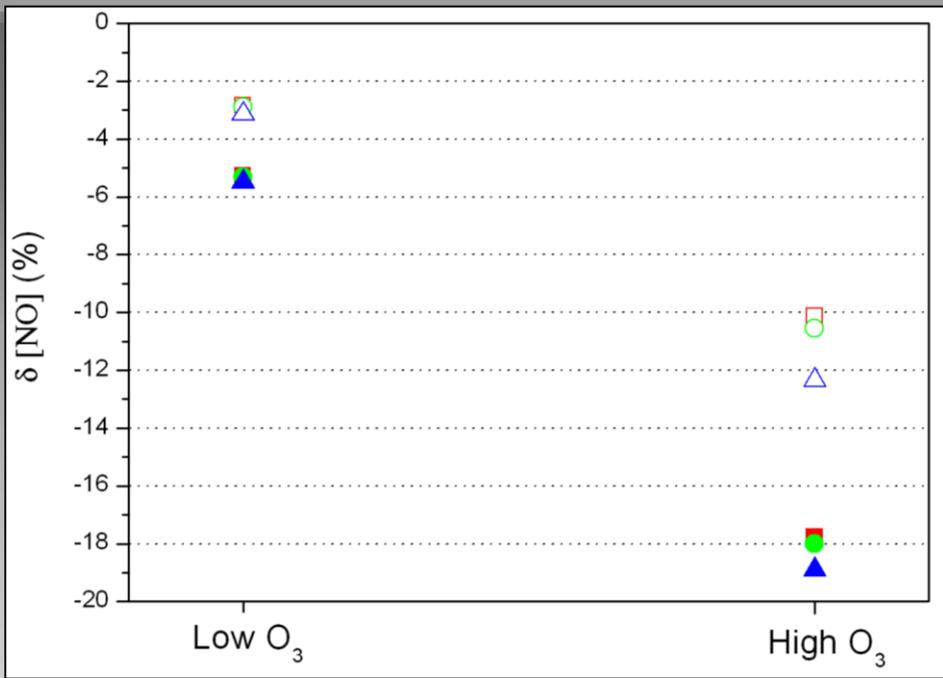
# Ozone

## Vertical profiles

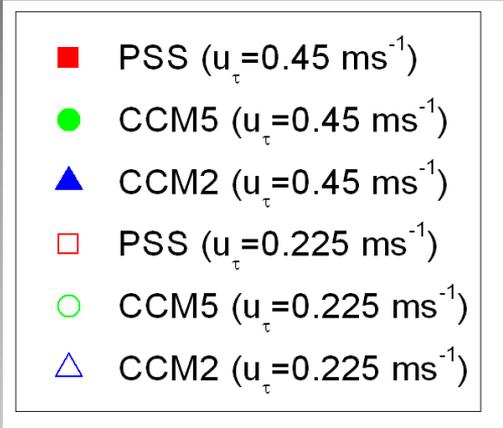
(solid line): High Ozone  
(dashed line): Low Ozone



- Horizontal spatial average of  $[NO]_N$  and  $[NO_2]_N$
- The same vertical profile: PSS and CCM5
- High O<sub>3</sub>: Importance of NO<sub>x</sub>/VOCs emission ( $[NO_2]_N$ )
- Low O<sub>3</sub>: the difference between chemical mechanism is insignificant

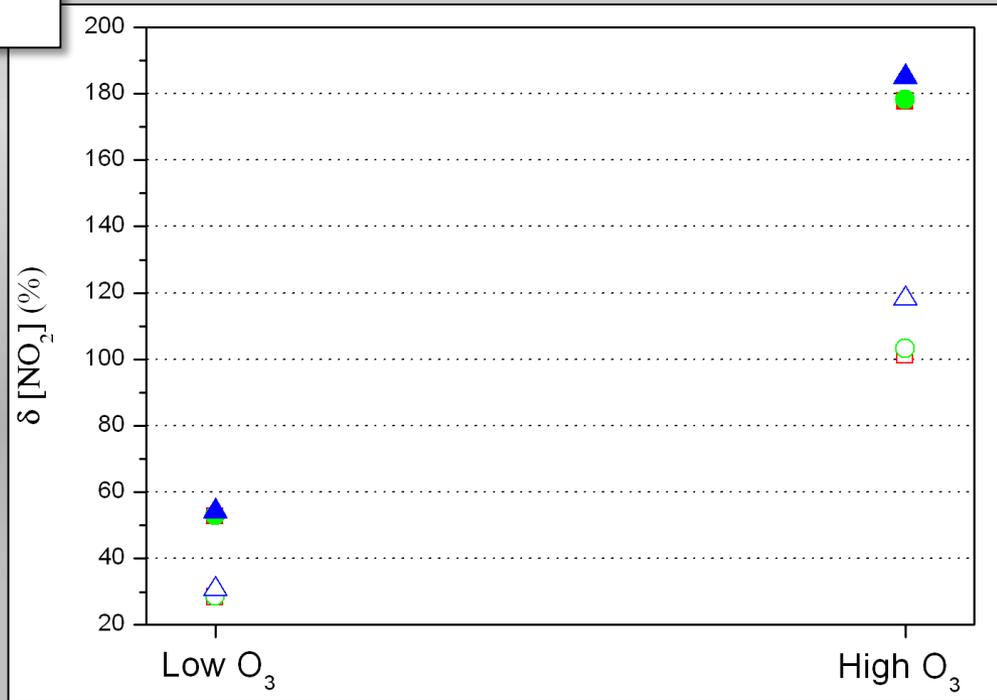


## 2D Geometry



- The average of  $\delta C$  below the canopy

$$\delta C = \frac{C_{norm} - C_{norm}(PS)}{C_{norm}(PS)}$$



# Conclusions

- ✓ The biggest change in  $[\text{NO}]$  and  $[\text{NO}_2]$  is obtained between chemical mechanisms and tracer (non-reactive)
- ✓ In the case of high  $[\text{O}_3]$ , the errors induced by the use of PSS are larger when the VOCs-to-NOx emission ratio increases → Lower  $[\text{NO}]$   
Higher  $[\text{NO}_2]$
- ✓ With lower  $[\text{O}_3]$  at the top of the domain,  $[\text{NO}]$  and  $[\text{NO}_2]$  can be simulated by a simple or complex chemical mechanisms due to the differences between mechanisms are negligible.
- ✓ The influence of a complex chemical mechanism is slightly smaller in 3D than 2D geometry since major ventilation is produced within the street.

**Thank you  
for your attention**



# **Additional Slides**

# Simulation Set up

## ❖ Top Conditions

- Constant concentration at the top →

Important role  
within the canyon

<b>NO</b>	16 ppb
<b>NO2</b>	35 ppb
<b>CO</b>	200 ppb
<b>SO2</b>	2 ppb

- **Ozone concentration** is computed using photostationary equilibrium and is dependent on zenith angle ( $\theta$ )

$$\left. \begin{array}{l} \theta = 45^\circ \\ \theta = 78^\circ \end{array} \right\} \rightarrow J_{\text{NO}_2} = A \exp(B/\cos(\theta)) \quad (\text{A and B are constant})$$
$$\downarrow$$
$$[O_3] = \frac{J_{\text{NO}_2} [\text{NO}_2]}{k [\text{NO}]}$$
$$\rightarrow \left\{ \begin{array}{l} O_3 = 39.8 \text{ ppb} \\ O_3 = 10.2 \text{ ppb} \end{array} \right.$$

# Simulation Set up

## ❖ Top Conditions

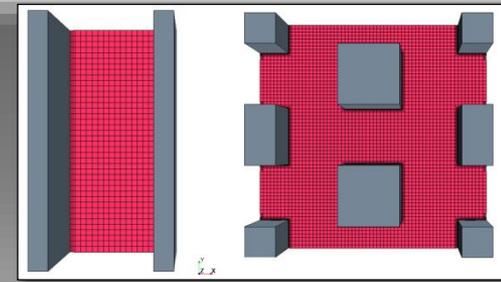
- **VOCs concentration** at the top change with emission ratio

	Emission scenarios	
	VOCs-to-NOx=1/5	VOCs-to-NOx=1/2
<b>NO</b>	16 ppb	16 ppb
<b>NO2</b>	35 ppb	35 ppb
<b>VOCs</b>	10.2 pbb	25.5 pbb

- Volumetric proportion within VOCs group are:

<b>OLE</b>	28.6 %
<b>ARO</b>	23.1 %
<b>ALK</b>	38.6%
<b>ALD</b>	4.0 %
<b>HCHO</b>	5.6 %

# Simulation Set up



## ❖ Traffic Emissions

- NOx fixed emissions:  $\left\{ \begin{array}{l} S_{\text{NO}} = 112 \mu\text{g m}^{-1}\text{s}^{-1} \\ S_{\text{NO}_2} = 17 \mu\text{g m}^{-1}\text{s}^{-1} \end{array} \right.$
- VOCs emissions  $\longrightarrow$  Complex Chemical Mechanism
- Some VOCs are joined in specific chemical groups
- VOCs-to-NOx emissions :  $\left\{ \begin{array}{l} \text{VOCs/NO}_x = 1/5 \quad (\text{in ppb}) \\ \text{VOCs/NO}_x = 1/2 \quad (\text{in ppb}) \end{array} \right.$
- Volumetric proportion within VOCs group are:

<b>OLE</b>	28.6 %
<b>ARO</b>	23.1 %
<b>ALK</b>	38.6%
<b>ALD</b>	4.0 %
<b>HCHO</b>	5.6 %

# Validation

## ❖ CFD Model

- Validated previously with tunnel measurements in:
  - Papers

## ❖ Complex Chemical Mechanism

- Validated previously with results of box model
- Experimental measurements